

---

## **APPENDIX B**

### **MEDIA CONCENTRATION CALCULATIONS**

**Table B1-1. Benzene Summary**

	Concentration from Project	Background Concentration <sup>1</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>2</sup>	Total Concentration Percent of ESL	Ecological Screening Quotient
Soil (mg/kg)	2.32E-08	N/A	N/A	2.55E-01	N/A	0.00
Water (mg/L)	1.79E-15	1.00E-03	1.00E-03	1.14E-01	0.88%	N/A
Sediment (mg/kg)	4.43E-15	N/A	N/A	1.42E-01	N/A	0.00

Notes:

<sup>1</sup> Water background concentration assumed to be the average concentration from water samples in or near Jefferson County, obtained from the IEP A on 01/19/11 via J. Schewe of Falcon Engineering.

<sup>2</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/reg5rcra/ca/guidance.htm>.

**Table B1-2. Benzene Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$	
<b>Cs</b>	<b>2.32E-08</b> Benzene concentration in soil (mg benzene/kg soil)
<b>tD</b>	<b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)
<b>Ds</b>	<b>1.28E-05</b> Deposition term (mg benzene/kg soil/yr)
$Ds = 100/(Z_n * BD) * [F_v(Dydv + Dywv) + (Dywp + Dydp) * (1 - F_v)]$	
	1.00E+02 Units conversion factor ( $m^2\text{-mg/cm}^2\text{-kg}$ )
$Z_n$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$	1.00E+00 Fraction of benzene air concentration in vapor phase (SLERA Protocol Table A-2-18)
$Dydv + Dywv$	3.83E-06 Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2\text{-yr}$ )
$Dywp + Dydp$	- Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2\text{-yr}$ )
<b>ks</b>	<b>5.49E+02</b> benzene soil loss constant due to all soil processes (yr-1)
$ks = k_{sg} + k_{se} + k_{sr} + k_{sl} + k_{sv}$	
$k_{sg}$	3.89E+00 Benzene loss constant due to biotic and abiotic degradation (yr-1) (SLERA Protocol Table A-2-18)
$k_{se}$	0.00E+00 Benzene loss constant due to soil erosion (yr-1) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$	1.12E+00 Benzene loss constant due to surface runoff (yr-1)
$k_{sl}$	0.00E+00 Benzene loss constant due to leaching (yr-1)
$k_{sv}$	5.44E+02 Benzene loss constant due to volatilization (yr-1)
<b>ksr</b>	<b>1.12E+00</b> Benzene loss constant due to surface runoff (yr-1)
$k_{sr} = RO / (\theta_{sw} * Z_n) * \{1/[1 + (Kd_s * BD/\theta_{sw})]\}$	
RO	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_n$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	6.20E-01 Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-18)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b>ksl</b>	<b>0.00E+00</b> Benzene loss constant due to leaching (yr-1)
$k_{sl} = (P + I - RO - E_v) / \{\theta_{sw} * Z_n * [1.0 + (BD * Kd_s / \theta_{sw})]\}$	
P	1.02E+02 Annual average precipitation (cm/yr) (NOAA, Local Climatological Data, Normal Yearly Precipitation)
I	0.00E+00 Average annual irrigation (cm/yr) (Baes Reference to SLERA Protocol Table B-1-5, Assumed due to low
	Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
RO	2.54E+01 Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$E_v$	7.62E+01 Average annual evapotranspiration (cm/yr) (Baes Reference to SLERA Protocol Table B-1-5)
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_n$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Kd_s$	6.20E-01 Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-18)
<b>ksv</b>	<b>5.44E+02</b> Benzene loss constant due to volatilization (yr-1)
$k_{sv} = [3.1536 \times 10^7 * H / (Z_n * Kd_s * R * T_a * BD)] * [D_a / Z_n] * [1 - (BD/\rho_s) - \theta_{sw}]$	
	3.15E+07 Units conversion factor (s/yr)
H	5.49E-03 Henry's Law constant ( $atm\text{-m}^3/mol$ ) (SLERA Protocol Table A-2-18)
$Z_n$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	6.20E-01 Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-18)
R	8.21E-05 Universal gas constant ( $atm\text{-m}^3/mol\text{-K}$ )
$T_a$	2.98E+02 Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$\rho_s$	2.70E+00 Solids particle density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$D_a$	1.17E-01 Diffusivity of Benzene in air ( $cm^2/s$ ) (SLERA Protocol Table A-2-18)
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

**Table B1-3. Benzene Load to Water Body**

$L_T = L_{DEP} + L_{DVC} + L_{RI} + L_R + L_E + L_I$	
$L_T$	3.24E+02 Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DVC}$	2.29E+02 Total (wet and dry) particle phase and wet vapor phase COPC direct deposition load to water body (g/yr)
$L_{DVC} = A_w * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
A <sub>w</sub>	5.98E+07 Water body surface area (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
F <sub>v</sub>	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-18)
Dwvp	3.83E-06 Yearly average wet deposition from vapor phase from model (over water body) (g/m <sup>2</sup> ·yr)
Dwdpp	0.00E+00 Yearly average total (wet and dry) deposition from particle phase from model (over water body) (g/m <sup>2</sup> ·yr)
$L_{DIF}$	5.58E-05 Vapor phase COPC diffusion (dry deposition) load to water body (g/yr)
$L_{DIF} = (K_{tr} * F_v * Cvp * 1.0 \times 10^{-6}) / (H(RT_{wk}))$	
K <sub>tr</sub>	8.69E+02 Overall transfer rate coefficient (m/yr)
F <sub>v</sub>	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-18)
Cvp	1.44E-02 Yearly average air concentration from vapor phase from model (over water body) (mg/m <sup>3</sup> )
H	5.49E-03 Henry's Law constant (atm·m <sup>3</sup> /mol) (SLERA Protocol Table A-2-18)
R	8.21E-05 Universal gas constant (atm·m <sup>3</sup> /mol·K)
T <sub>wk</sub>	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_{RI}$	8.35E+01 Runoff load from impervious sources (g/yr)
$L_{RI} = A_I * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
F <sub>v</sub>	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-18)
Dwvp	3.83E-06 Yearly average wet deposition from vapor phase from model (over water body) (g/m <sup>2</sup> ·yr)
Dwdpp	0.00E+00 Yearly average total (wet and dry) deposition from particle phase from model (over water body) (g/m <sup>2</sup> ·yr)
A <sub>I</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$L_R$	1.17E+01 Runoff load from pervious sources (g/yr)
$L_R = RO * (A_L - A_I) * [(Cs * BD) / (θrw + Kdr * BD)] * 0.01$	
RO	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k-regionalsum.html</a> )
A <sub>L</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
A <sub>I</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
Cs	2.32E-08 COPC concentration in soil (mg/kg)
BD	1.50E+00 Soil bulk density (g/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-5)
θ <sub>rw</sub>	2.00E-01 Soil volumetric water content (mL/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-5)
Kd <sub>r</sub>	6.20E-01 Soil-water partition coefficient (cm <sup>3</sup> /g) (SLERA Protocol Table A-2-18)
	1.00E-02 Units conversion factor (kg·cm <sup>3</sup> /mg·m <sup>3</sup> )
$L_E$	1.85E-01 Soil erosion load (g/yr)
$L_E = X_e * (A_L - A_I) * SD * ER * [(Cs * Kdr * BD) / (θrw + Kdr * BD)] * 0.001$	
X <sub>e</sub>	2.54E+01 Unit soil loss (kg/m <sup>2</sup> ·yr)
A <sub>L</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
A <sub>I</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
SD	8.55E-02 Watershed sediment delivery ratio (unitless)
ER	3.00E+00 Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for Inorganic COPC's and 3 for Organic COPC's)
Cs	2.32E-08 COPC concentration in soil (mg/kg)
Kd <sub>r</sub>	6.20E-01 Soil-water partition coefficient (cm <sup>3</sup> /g) (SLERA Protocol Table A-2-18)
BD	1.50E+00 Soil bulk density (g/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-6)
θ <sub>rw</sub>	2.00E-01 Soil volumetric water content (mL/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-6)
	1.00E-03 Units conversion factor (g/mg)
$L_I$	0.00E+00 Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
$X_r$	2.44E+01 Unit soil loss (kg/m <sup>2</sup> ·yr)
$X_r = RF * K * LS * C * PF * (907.18/4047)$	
RF	3.00E+02 Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor (yr <sup>-1</sup> ) (Highest value from range listed in SLERA Protocol Table B-2-7)
K	3.60E-01 USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7)
LS	1.50E+00 USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7)
C	7.00E-01 USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7)
PF	1.00E+00 USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place)
	9.07E+02 Units conversion factor (kg/ton)
	4.05E+03 Units conversion factor (m <sup>3</sup> /acre)
SD	8.55E-02 Watershed sediment delivery ratio (unitless)
$SD = a * (A_L)^b$	
a	1.20E+00 Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>b</sup> )
A <sub>L</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
b	1.25E-01 Empirical slope coefficient (unitless) (default value from Table B-2-8)

<sup>1</sup>Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>2</sup>Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>3</sup>Watershed area estimated to be receiving COPC is between 10 and 100 square miles.

**Table B1-4. Benzene Water Body Concentration**

$C_{w,td} = L_f / [Vf_w * f_{wc} + k_{w1} * A_w * (d_{sc} + d_{ss})]$
$C_{w,tot}$ <b>2.04E-15</b> Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_f$ <b>3.24E+02</b> Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_w$ <b>1.32E+08</b> Average volumetric flow rate through water body (m <sup>3</sup> /yr)
$f_{wc}$ <b>8.15E-01</b> Fraction of total water body COPC concentration that occurs in the water column (unitless)
$L_{sc} = [(1 + Kd_{sc} * TSS * 10^{-5}) * d_{sc}/d_z] / [(1 + Kd_{ss} * TSS * 10^{-5}) * d_{ss}/d_z + (q_s + Kd_{ss} * BS) * d_z/d_z]$
$f_{ss} = 1 - f_{wc}$
$f_{ss}$ <b>1.85E-01</b> Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{sc}$ <b>4.65E+00</b> Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-18)
$TSS$ <b>3.00E+02</b> Total suspended solids concentration (mg/L) (High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
<b>1.00E-06</b> Units conversion factor (kg/mg)
$d_{sc}$ <b>4.05E-01</b> Depth of water column (m) <sup>1</sup>
$d_{ss}$ <b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$ <b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{sc} + d_{ss}$ )
$BS$ <b>1.00E-06</b> Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)
$q_s$ <b>6.00E-01</b> Bed sediment porosity ( $L_{soil}/L_{sediment}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{ss}$ <b>2.48E+00</b> Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-18)
$k_{wt}$ <b>6.09E+09</b> Overall total water body COPC dissipation rate constant (yr <sup>-1</sup> ) <sup>3</sup>
$k_{wt} = f_{wc} * k_v * k_b * k_p$
$f_{wc}$ <b>8.15E-01</b> Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_v$ <b>1.99E+03</b> Water column volatilization rate constant (yr <sup>-1</sup> )
$f_{ss}$ <b>1.85E-01</b> Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_b$ <b>3.28E+10</b> Benthic burial rate constant (yr <sup>-1</sup> )
$A_w$ <b>5.98E+07</b> Water body surface area (m <sup>2</sup> )
$k_p$ <b>1.99E+03</b> Water column volatilization rate constant (yr <sup>-1</sup> )
$k_v = K_v / [d_z * (1 + Kd_{ss} * TSS * 10^{-5})]$
$K_v$ <b>8.69E+02</b> Overall COPC transfer rate coefficient (m/yr)
$d_{sc}$ <b>4.05E-01</b> Depth of water column (m)
$d_{ss}$ <b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$ <b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{sc} + d_{ss}$ )
$Kd_{ss}$ <b>4.65E+00</b> Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-18)
$TSS$ <b>3.00E+02</b> Total suspended solids concentration (mg/L)
<b>1.00E-06</b> Units conversion factor (kg/mg)
$K_v$ <b>8.69E+02</b> Overall COPC transfer rate coefficient (m/yr)
$K_v = (K_{Lc}^{-1} + [K_{Lc} * H/(R * T_{wk})]^{1/2})^{-1} * q^{(T_{wk} - 29)} \quad (T_{wk} > 29)$
$K_{Lc}$ <b>8.43E+02</b> Liquid-phase transfer coefficient (m/yr)
$K_{Gc}$ <b>3.65E+04</b> Gas-phase transfer coefficient (m/yr)
$H$ <b>5.49E-03</b> Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-18)
$R$ <b>8.21E-05</b> Universal gas constant (atm-m <sup>3</sup> /mol-K)
$T_{wk}$ <b>2.98E+02</b> Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
$q$ <b>1.03E+00</b> Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_{Lc}$ <b>8.43E+02</b> Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_L = \text{SQRT}((10^{-4} * D_w * u / d_z) * 3.1536 * 10^7)$
$D_w$ <b>1.02E-05</b> Diffusivity of COPC in water (cm <sup>2</sup> /s) (SLERA Protocol Table A-2-175)
$u$ <b>3.05E-01</b> Current velocity (m/s) <sup>4</sup>
$d_z$ <b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{sc} + d_{ss}$ )
<b>3.15E+07</b> Units conversion constant (s/yr)
$K_{Gc}$ <b>3.65E+04</b> Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$k_b$ <b>3.28E+10</b> Benthic burial rate constant (yr <sup>-1</sup> )
$k_b = [X_s * A_t * SD * 10^3 - Vf_w * TSS / (A_w * TSS)] * [TSS * 10^{-5} / (BS * d_{ss})]$
$X_s$ <b>2.54E+01</b> Unit soil loss (kg/m <sup>2</sup> /yr)
$A_t$ <b>1.51E+09</b> Total watershed area receiving COPC deposition (m <sup>2</sup> )
$SD$ <b>8.55E-02</b> Watershed sediment delivery ratio (unitless)
$Vf_w$ <b>1.32E+08</b> Average volumetric flow rate through water body (m <sup>3</sup> /yr)
$TSS$ <b>3.00E+02</b> Total suspended solids concentration (mg/L)
$A_w$ <b>5.98E+07</b> Water body surface area (m <sup>2</sup> )
$BS$ <b>1.00E-06</b> Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-16)
$d_{ss}$ <b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup>Assume pH = 8.0 based on water quality data provided by EPA Region 5

<sup>2</sup>Values found for data from Mississippi River near St. Louis range from 50-350 mg/L, therefore used high end of SLERA default range.

<sup>3</sup>Based on minimum depth required by Corps of Engineers

<sup>4</sup>Assume COPC does not dissipate based on Henry's Law constant of zero.

<sup>5</sup>Current velocity ranges from 3-7 ft/s based on information from several sources.

**Table B1-5. Benzene Concentration in Water Column**

$C_{wc\text{tot}} = f_{wc} * C_{w\text{tot}} * (d_{wc} + d_{bs}) / d_{wc}$		
<b><math>C_{wc\text{tot}}</math></b>	<b>1.79E-15</b>	Total COPC concentration in water column (mg/L)
$f_{wc}$	8.15E-01	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{w\text{tot}}$	2.04E-15	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B1-6. Benzene Dissolved Phase Water Concentration**

$C_{dw} = C_{wctot} / (1 + Kd_{sw} * TSS * 10^6)$		
<b>1.79E-15</b>	Dissolved phase water concentration (mg/L)	
$C_{wctot}$	1.79E-15	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	4.65E+00	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-18)
TSS	3.00E+02	Total suspended solids concentration (mg/L)

**Table B1-7. Benzene Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{hs}} * C_{\text{wtot}} * [Kd_{\text{bs}} / (q_{\text{bs}} + Kd_{\text{bs}} * BS)] * [(d_{\text{wc}} + d_{\text{bs}}) / d_{\text{bs}}]$						
$C_{\text{sed}}$	<b>4.43E-15</b>	COPC concentration in bed sediment (mg/kg)				
$f_{\text{hs}}$	<b>1.85E-01</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)				
$C_{\text{wtot}}$	<b>2.04E-15</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)				
$Kd_{\text{bs}}$	<b>2.48E+00</b>	Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-18)				
$q_{\text{bs}}$	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}} / L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)				
$BS$	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)				
$d_{\text{wc}}$	<b>4.05E-01</b>	Depth of water column (m)*				
$d_{\text{bs}}$	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)				

**Table B2-1. Methylene Chloride Summary**

	<b>Concentration from Project</b>	<b>Background Concentration</b>	<b>Total Concentration (Background &amp; Project)</b>	<b>Ecological Screening Level<sup>1</sup></b>	<b>Total Concentration Percent of ESL</b>	<b>Ecological Screening Quotient</b>
Soil (mg/kg)	1.25E-06	N/A	N/A	4.05E+00	N/A	0.00
Water (mg/L)	6.04E-13	N/A	N/A	9.40E-01	N/A	0.00
Sediment (mg/kg)	2.42E-13	N/A	N/A	1.59E-01	N/A	0.00

Notes:

<sup>1</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/reg5rcra/ca/guidance.htm>.

**Table B2-2. Methylene Chloride Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$		
<b>Cs</b>	<b>1.25E-06</b> Methylene chloride concentration in soil (mg methylene chloride/kg soil)	
<b>tD</b>	<b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)	
<b>Ds</b>	<b>1.37E-03</b> Deposition term (mg methylene chloride/kg soil/yr)	
$D_s = 100/(Z_s * BD) * [F_v(Dydv + Dywv) + (Dyw + Dydp) * (1 - F_v)]$		
	1.00E+02	Units conversion factor ( $m^2 \cdot mg/cm^2 \cdot kg$ )
$Z_s$	2.00E+01	Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00	Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$	1.00E+00	Fraction of methylene chloride air concentration in vapor phase (SLERA Protocol Table A-2-143)
$Dydv + Dywv$	4.11E-04	Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2 \cdot yr$ )
$Dyw + Dydp$	-	Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2 \cdot yr$ )
<b>ks</b>	<b>1.10E+03</b> Methylene chloride soil loss constant due to all soil processes ( $yr^{-1}$ )	
$ks = k_{sg} + k_{se} + k_{sr} + k_{sl} + k_{sv}$		
$k_{sg}$	9.03E+00	Methylene chloride loss constant due to biotic and abiotic degradation ( $yr^{-1}$ ) (SLERA Protocol Table A-2-143)
$k_{se}$	0.00E+00	Methylene chloride loss constant due to soil erosion ( $yr^{-1}$ ) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$	3.63E+00	Methylene chloride loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sl}$	0.00E+00	Methylene chloride loss constant due to leaching ( $yr^{-1}$ )
$k_{sv}$	1.09E+03	Methylene chloride loss constant due to volatilization ( $yr^{-1}$ )
<b>ksr</b>	<b>3.63E+00</b> Methylene chloride loss constant due to surface runoff ( $yr^{-1}$ )	
$ksr = RO / (\theta_{sw} * Z_s) * \{1/[1 + (Kd_s * BD/\theta_{sw})]\}$		
$RO$	2.54E+01	Average annual surface runoff ( $cm/yr$ ) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$\theta_{sw}$	2.00E-01	Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_s$	2.00E+01	Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	1.00E-01	Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-143)
$BD$	1.50E+00	Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b>ksl</b>	<b>0.00E+00</b> Methylene chloride loss constant due to leaching ( $yr^{-1}$ )	
$ksl = (P + I - RO - E_v) / \{\theta_{sw} * Z_s * [1.0 + (BD * Kd_s / \theta_{sw})]\}$		
$P$	1.02E+02	Annual average precipitation ( $cm/yr$ ) (NOAA, Local Climatological Data, Normal Yearly Precipitation)
$I$	0.00E+00	Average annual irrigation ( $cm/yr$ ) (Baes Reference to SLERA Protocol Table B-1-5, Assumed due to low irrigation)
$RO$	2.54E+01	Average annual surface runoff ( $cm/yr$ ) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$E_v$	7.62E+01	Average annual evapotranspiration ( $cm/yr$ ) (Baes Reference to SLERA Protocol Table B-1-5)
$\theta_{sw}$	2.00E-01	Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_s$	2.00E+01	Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00	Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Kd_s$	1.00E-01	Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-143)
<b>ksv</b>	<b>1.09E+03</b> Methylene chloride loss constant due to volatilization ( $yr^{-1}$ )	
$ksv = [3.1536 \times 10^7 * H / (Z_s * Kd_s * R * T_a * BD)] * [D_a / Z_s] * [1 - (BD/p_a) - \theta_{sw}]$		
	3.15E+07	Units conversion factor ( $s/yr$ )
$H$	2.38E-03	Henry's Law constant ( $atm \cdot m^3/mol$ ) (SLERA Protocol Table A-2-143)
$Z_s$	2.00E+01	Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	1.00E-01	Soil-water partition coefficient ( $mL/g$ ) (SLERA Protocol Table A-2-143)
$R$	8.21E-05	Universal gas constant ( $atm \cdot m^3/mol \cdot K$ )
$T_a$	2.98E+02	Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
$BD$	1.50E+00	Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$p_a$	2.70E+00	Solids particle density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$D_a$	8.69E-02	Diffusivity of methylene chloride in air ( $cm^2/s$ ) (SLERA Protocol Table A-2-143)
$\theta_{sw}$	2.00E-01	Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

**Table B2-3. Methylene Chloride Load to Water Body**

$L_T = L_{DWP} + L_{DF} + L_{RI} + L_R + L_E + L_I$
$L_T = 3.56E+04$ Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DWP} = 2.46E+04$ Total (wet and dry) particle phase and wet vapor phase COPC direct deposition load to water body (g/yr)
$L_{DF} = A_w * [F_v * Dwvp + (1-F_v) * Dwdpp]$
$A_w = 5.98E+07$ Water body surface area ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $F_v = 1.00E+00$ Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-143) $Dwvp = 4.11E-04$ Yearly average wet deposition from vapor phase from model (over water body) ( $kg/m^2 \cdot yr$ ) $Dwdpp = 0.00E+00$ Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $kg/m^2 \cdot yr$ )
$L_{DWP} = 5.02E-03$ Vapor phase COPC diffusion (dry deposition) load to water body (g/yr)
$L_{DF} = (K_c * F_v * Cvp * (1.0 \times 10^{-5}) * (H/(R*T_{sk}))$
$K_c = 3.40E+02$ Overall transfer rate coefficient (m/yr) $F_v = 1.00E+00$ Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-143) $Cvp = 5.82E-01$ Yearly average air concentration from vapor phase from model (over water body) ( $mg/m^3$ ) $H = 2.38E-03$ Henry's Law constant ( $atm \cdot m^3/mol$ ) (SLERA Protocol Table A-2-143) $R = 8.21E-05$ Universal gas constant ( $atm \cdot m^3/mol \cdot K$ ) $T_{sk} = 2.98E+02$ Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_{RI} = 8.98E+03$ Runoff load from impervious sources (g/yr)
$L_{RI} = A_I * [F_v * Dwvp + (1-F_v) * Dwdpp]$
$F_v = 1.00E+00$ Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-143) $Dwvp = 4.11E-04$ Yearly average wet deposition from vapor phase from model (over water body) ( $kg/m^2 \cdot yr$ ) $Dwdpp = 0.00E+00$ Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $kg/m^2 \cdot yr$ ) $A_I = 2.18E+07$ Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]])
$L_R = 2.02E+03$ Runoff load from pervious sources (g/yr)
$L_R = RO * (A_L - A_I) * [(Cs * BD)/(I_{so} + Kd * BD)] * 0.01$
$RO = 2.54E+01$ Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/fa/fa730/ch_1/k-regionalsum.html">http://pubs.usgs.gov/fa/fa730/ch_1/k-regionalsum.html</a> ) $A_L = 1.51E+09$ Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $A_I = 2.18E+07$ Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $Cs = 1.25E-06$ COPC concentration in soil ( $mg/kg$ ) $BD = 1.50E+00$ Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-5) $I_{so} = 2.00E-01$ Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-5) $Kd = 1.00E-01$ Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-143) $1.00E-02$ Units conversion factor ( $kg \cdot cm^2/mg \cdot m^2$ )
$L_E = 5.19E+00$ Soil erosion load (g/yr)
$L_E = X_e * (A_L - A_I) * SD * ER * [(Cs * Kd * BD)/(I_{so} + Kd * BD)] * 0.001$
$X_e = 2.54E+01$ Unit soil loss ( $kg/m^2 \cdot yr$ ) $A_L = 1.51E+09$ Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $A_I = 2.18E+07$ Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $SD = 8.55E-02$ Watershed sediment delivery ratio (unitless) $ER = 3.00E+00$ Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for Inorganic COPC's and 3 for Organic COPC's) $Cs = 1.25E-06$ COPC concentration in soil ( $mg/kg$ ) $Kd = 1.00E-01$ Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-143) $BD = 1.50E+00$ Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-6) $I_{so} = 2.00E-01$ Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-6) $1.00E-03$ Units conversion factor ( $kg/mg$ )
$L_I = 0.00E+00$ Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
$X_e = 2.54E+01$ Unit soil loss ( $kg/m^2 \cdot yr$ )
$X_e = RF * K * LS * C * PF * (907.18/4047)$
$RF = 3.00E+02$ Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor ( $yr^{-1}$ ) (Highest value from range listed in SLERA Protocol Table B-2-7) $K = 3.60E-01$ USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7) $LS = 1.50E+00$ USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7) $C = 7.00E-01$ USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7) $PF = 1.00E+00$ USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place) $9.07E+02$ Units conversion factor ( $kg/ion$ ) $4.05E+03$ Units conversion factor ( $m^3/acre$ )
$SD = 8.55E-02$ Watershed sediment delivery ratio (unitless)
$SD = a * (A_L)^b$
$a = 1.20E+00$ Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>a</sup> ) $A_L = 1.51E+09$ Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html">http://www.agr.state.il.us/gis/landcover99-00.html</a> [class accessed [12/06/2010]]) $b = 1.25E-01$ Empirical slope coefficient (unitless) (default value from Table B-2-8)

<sup>a</sup>Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>b</sup>Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>1</sup>Watershed area estimated to be receiving COPC is between 10 and 100 square miles.

**Table B2-4. Methylene Chloride Water Body Concentration**

$C_{w\text{tot}} = L_T / [Vf_w \cdot f_{w,c} + k_{w,c} \cdot A_w \cdot (d_{w,c} + d_{w,s})]$	
$C_{w\text{tot}}$	6.04E-13 Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_T$	3.56E+04 Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_w$	1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$f_{w,c}$	9.31E-01 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$f_{w,c} = [(1 + Kd_{ws} \cdot \text{TSS} \cdot 10^{-6}) \cdot d_{w,c}/d_z] / [(1 + Kd_{ws} \cdot \text{TSS} \cdot 1 \times 10^{-6}) \cdot d_{w,c}/d_z + (q_{bs} + Kd_{ws} \cdot \text{BS}) \cdot d_{w,s}/d_z]$	
$f_{w,s}$	6.89E-02 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{ws}$	7.50E-01 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-143)
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L) (High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
	1.00E-06 Units conversion factor (kg/mg)
$d_{w,c}$	4.05E-01 Depth of water column ( $\text{m}^3$ )
$d_{w,s}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{w,c} + d_{w,s}$ )
$BS$	1.00E+00 Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)
$q_{bs}$	6.00E-01 Bed sediment porosity ( $L_{\text{water}}/L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{bs}$	4.00E-01 Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-143)
$k_{w,t}$	2.26E+09 Overall total water body COPC dissipation rate constant ( $\text{yr}^{-1}$ ) <sup>1</sup>
$k_{w,t} = f_{w,c} \cdot k_{w,c} + f_{w,s} \cdot k_s$	
$f_{w,c}$	9.31E-01 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_{w,c}$	1.93E+03 Water column volatilization rate constant ( $\text{yr}^{-1}$ )
$f_{w,s}$	6.89E-02 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_s$	3.28E+10 Benthic burial rate constant ( $\text{yr}^{-1}$ )
$A_w$	5.98E+07 Water body surface area ( $\text{m}^2$ )
$k_v$	1.93E+03 Water column volatilization rate constant ( $\text{yr}^{-1}$ )
$k_v = K_v / [d_z \cdot (1 + Kd_{ws} \cdot \text{TSS} \cdot 10^{-6})]$	
$K_v$	8.40E+02 Overall COPC transfer rate coefficient (m/yr)
$d_{w,c}$	4.05E-01 Depth of water column (m)
$d_{w,s}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{w,c} + d_{w,s}$ )
$Kd_{ws}$	7.50E-01 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-143)
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L)
	1.00E-06 Units conversion factor (kg/mg)
$K_v$	8.40E+02 Overall COPC transfer rate coefficient (m/yr)
$K_v = (K_t^{-1} + [K_t \cdot H/(R \cdot T_{sk})])^{-1} \cdot q^{(T_{sk} - 20)}$	
$K_t$	9.33E+02 Liquid-phase transfer coefficient (m/yr)
$K_g$	3.65E+04 Gas-phase transfer coefficient (m/yr)
$H$	2.38E-03 Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-143)
$R$	8.21E-05 Universal gas constant (atm-m <sup>3</sup> /mol-K)
$T_{sk}$	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
$q$	1.03E+00 Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_L$	9.33E+02 Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_L = \text{SQRT}(10^{-4} \cdot D_w \cdot u / d_z) \cdot 3.1536 \times 10^7$	
$D_w$	1.25E-05 Diffusivity of COPC in water ( $\text{cm}^2/\text{s}$ ) (SLERA Protocol Table A-2-143)
$u$	3.05E-01 Current velocity ( $\text{m/s}$ ) <sup>5</sup>
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{w,c} + d_{w,s}$ )
	3.15E+07 Units conversion constant (s/yr)
$K_g$	3.65E+04 Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$K_b$	3.28E+10 Benthic burial rate constant ( $\text{yr}^{-1}$ )
$k_b = [X_c \cdot A_t \cdot SD \cdot 10^3 - Vf_w \cdot \text{TSS} / (A_w \cdot \text{TSS})] \cdot [\text{TSS} \cdot 10^{-6} / (\text{BS} \cdot d_{w,s})]$	
$X_c$	2.54E+01 Unit soil loss ( $\text{kg/m}^2 \cdot \text{yr}$ )
$A_t$	1.51E+09 Total watershed area receiving COPC deposition ( $\text{m}^2$ )
$SD$	8.55E-02 Watershed sediment delivery ratio (unitless)
$Vf_w$	1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L)
$A_w$	5.98E+07 Water body surface area ( $\text{m}^2$ )
$BS$	1.00E+00 Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-16)
$d_{w,s}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup>Assume pH = 8.0 based on water quality data provided by EPA Region 5

<sup>2</sup>Values found for data from Mississippi River near St. Louis range from 50-350 mg/L, therefore used high end of SLERA default range.

<sup>3</sup>Based on minimum depth required by Corps of Engineers

<sup>4</sup>Assume COPC does not dissipate based on Henry's Law constant of zero.

<sup>5</sup>Current velocity ranges from 3-7 ft/s based on information from several sources.

**Table B2-5. Methylene Chloride Concentration in Water Column**

$C_{wc\text{tot}} = f_{wc} * C_{w\text{tot}} * (d_{wc} + d_{bs}) / d_{wc}$		
<b>6.04E-13</b>	Total COPC concentration in water column (mg/L)	
$f_{wc}$	9.31E-01	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{w\text{tot}}$	6.04E-13	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B2-6. Methylene Chloride Dissolved Phase Water Concentration**

$C_{dw} = C_{wctot} / (1 + Kd_{sw} * TSS * 10^6)$		
$C_{dw}$	<b>6.04E-13</b>	Dissolved phase water concentration (mg/L)
$C_{wctot}$	6.04E-13	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	7.50E-01	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-143)
TSS	3.00E+02	Total suspended solids concentration (mg/L)

**Table B2-7. Methylene Chloride Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{bs}} * C_{\text{wiot}} * [Kd_{\text{bs}} / (q_{\text{bs}} + Kd_{\text{bs}} * BS)] * [(d_{\text{wc}} + d_{\text{bs}}) / d_{\text{bs}}]$				
$C_{\text{sed}}$	<b>2.42E-13</b>	COPC concentration in bed sediment (mg/kg)		
$f_{\text{bs}}$	<b>6.89E-02</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)		
$C_{\text{wiot}}$	<b>6.04E-13</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)		
$Kd_{\text{bs}}$	<b>4.00E-01</b>	Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-143)		
$q_{\text{bs}}$	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}} / L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)		
BS	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)		
$d_{\text{wc}}$	<b>4.05E-01</b>	Depth of water column (m)*		
$d_{\text{bs}}$	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)		

**Table B3-1. Toluene Summary**

	Concentration from Project	Background Concentration <sup>1</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>2</sup>	Project Increase Percent of ESL	Ecological Screening Quotient
Soil (mg/kg)	1.86E-06	N/A	N/A	5.45E+00	N/A	0.00
Water (mg/L)	3.07E-14	1.00E-03	1.00E-03	2.53E-01	0.40%	N/A
Sediment (mg/kg)	1.72E-13	N/A	N/A	1.22E+00	N/A	0.00

Notes:

<sup>1</sup> Water background concentration assumed to be the average concentration from water samples in or near Jefferson County, obtained from the IEPA on 01/19/11 via J. Schewe of Falcon Engineering.

<sup>2</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/reg5rcra/ca/guidance.htm>.

**Table B3-2. Toluene Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$	
<b>Cs</b>	<b>1.86E-06</b> Toluene concentration in soil (mg toluene/kg soil)
<b>tD</b>	<b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)
<b>Ds</b>	<b>4.37E-04</b> Deposition term (mg toluene/kg soil/yr)
$D_s = 100/(Z_s * BD) * [F_v (Dydv + Dywv) + (Dywp + Dydp) * (1 - F_v)]$	
1.00E+02	Units conversion factor ( $m^2\text{-mg/cm}^2\text{-kg}$ )
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$	1.00E+00 Fraction of toluene air concentration in vapor phase (SLERA Protocol Table A-2-185)
Dydv + Dywv	1.31E-04 Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2\text{-yr}$ )
Dywp + Dydp	- Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2\text{-yr}$ )
<b>ks</b>	<b>2.36E+02</b> Toluene soil loss constant due to all soil processes ( $yr^{-1}$ )
$k_s = k_{sg} + k_{se} + k_{sr} + k_{sl} + k_{sv}$	
$k_{sg}$	1.15E+01 Toluene loss constant due to biotic and abiotic degradation ( $yr^{-1}$ ) (SLERA Protocol Table A-2-185)
$k_{se}$	0.00E+00 Toluene loss constant due to soil erosion ( $yr^{-1}$ ) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$	5.52E-01 Toluene loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sl}$	0.00E+00 Toluene loss constant due to leaching ( $yr^{-1}$ )
$k_{sv}$	2.24E+02 Toluene loss constant due to volatilization ( $yr^{-1}$ )
<b>ksr</b>	<b>5.52E-01</b> Toluene loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sr} = RO / (\theta_{sw} * Z_s) * \{1/[1 + (Kd_s * BD/\theta_{sw})]\}$	
RO	2.54E+01 Average annual surface runoff (cm/yr) (USGS)
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
Kd <sub>s</sub>	1.40E+00 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-185)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b>ksl</b>	<b>0.00E+00</b> Toluene loss constant due to leaching ( $yr^{-1}$ )
$k_{sl} = (P + I - RO - E_v) / \{\theta_{sw} * Z_s * [1.0 + (BD * Kd_s / \theta_{sw})]\}$	
P	1.02E+02 Annual average precipitation (cm/yr) (NOAA)
I	0.00E+00 Average annual irrigation (cm/yr) (Assumed due to low irrigation percentage in Illinois)
RO	2.54E+01 Average annual surface runoff (cm/yr)
$E_v$	7.62E+01 Average annual evapotranspiration (cm/yr)
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
Kd <sub>s</sub>	1.40E+00 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-185)
<b>ksv</b>	<b>2.24E+02</b> Toluene loss constant due to volatilization ( $yr^{-1}$ )
$k_{sv} = [3.1536 \times 10^7 * H / (Z_s * Kd_s * R * T_a * BD)] * [D_g / Z_s] * [1 - (BD/\rho_s) - \theta_{sw}]$	
3.15E+07	Units conversion factor (s/yr)
H	6.13E-03 Henry's Law constant ( $atm\cdot m^3/mol$ ) (SLERA Protocol Table A-2-185)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
Kd <sub>s</sub>	1.40E+00 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-185)
R	8.21E-05 Universal gas constant ( $atm\cdot m^3/mol\cdot K$ )
$T_a$	2.98E+02 Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
BD	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$\rho_s$	2.70E+00 Solids particle density ( $g/cm^3$ ) ( default value from SLERA Protocol Table B-1-6)
$D_g$	9.72E-02 Diffusivity of toluene in air ( $cm^2/s$ ) ( SLERA Protocol Table A-2-185)
$\theta_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

**Table B3-3. Toluene Load to Water Body**

$L_T = L_{DWP} + L_{DFP} + L_{RI} + L_R + L_E + L_I$	
$L_T$	<b>1.12E+04</b> Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DFP}$	<b>7.85E+03</b> Total (wet and dry) particle phase and wet vapor phase COPC direct deposition load to water body (g/yr)
$L_{DFP} = A_w * [F_v * Dwvp + (1-F_v) * Dwdp]$	
$A_w$	5.98E+07 Water body surface area ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$F_v$	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-185)
$Dwvp$	1.31E-04 Yearly average wet deposition from vapor phase from model (over water body) ( $g/m^2 \cdot yr$ )
$Dwdp$	0.00E+00 Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$L_{DFP}$	<b>2.09E-03</b> Vapor phase COPC diffusion (dry deposition) load to water body (g/yr)
$L_{DFP} = (K_{cv} * F_v * Cvp * 1.0 * 10^6 * V / (H * R * T_{wv}))$	
$K_{cv}$	8.38E+02 Overall transfer rate coefficient ( $m/yr$ )
$F_v$	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-185)
$Cvp$	6.25E-01 Yearly average air concentration from vapor phase from model (over water body) ( $mg/m^3$ )
$H$	6.13E-03 Henry's Law constant ( $atm \cdot m^3/mol$ ) (SLERA Protocol Table A-2-185)
$R$	8.21E-05 Universal gas constant ( $atm \cdot m^3/mol \cdot K$ )
$T_{wv}$	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_{RI}$	<b>2.87E+03</b> Runoff load from impervious sources (g/yr)
$L_{RI} = A_I * [F_v * Dwvp + (1-F_v) * Dwdp]$	
$F_v$	1.00E+00 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-185)
$Dwvp$	1.31E-04 Yearly average wet deposition from vapor phase from model (over water body) ( $g/m^2 \cdot yr$ )
$Dwdp$	0.00E+00 Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$A_I$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$L_R$	<b>4.58E+02</b> Runoff load from pervious sources (g/yr)
$L_R = RO * (A_I - A_p) * [(Cs * BD / (\theta_{rw} + Kd * BD)) * 0.01]$	
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/hb/hb70/ch_kk-regionalsum.html">http://pubs.usgs.gov/hb/hb70/ch_kk-regionalsum.html</a> )
$A_I$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$A_p$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$Cs$	1.86E-06 COPC concentration in soil ( $mg/kg$ )
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$\theta_{rw}$	2.00E-01 Soil volumetric water content ( $ml/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$Kd$	1.40E+00 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-185)
	1.00E-02 Units conversion factor ( $kg \cdot cm^2/mg \cdot m^3$ )
$L_E$	<b>1.65E+01</b> Soil erosion load (g/yr)
$L_E = X_e * (A_L - A_p) * SD * ER * [(Cs * Kd * BD) / (\theta_{rw} + Kd * BD)] * 0.001$	
$X_e$	2.54E+01 Unit soil loss ( $kg/m^2 \cdot yr$ )
$A_L$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ )
$A_p$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ )
$SD$	8.55E-02 Watershed sediment delivery ratio (unitless)
$ER$	3.00E+00 Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for Inorganic COPC's and 3 for Organic COPC's)
$Cs$	1.86E-06 COPC concentration in soil ( $mg/kg$ )
$Kd$	1.40E+00 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-185)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
$\theta_{rw}$	2.00E-01 Soil volumetric water content ( $ml/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
	1.00E-03 Units conversion factor ( $g/mg$ )
$L_I$	<b>0.00E+00</b> Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
$X_e$	<b>2.54E+01</b> Unit soil loss ( $kg/m^2 \cdot yr$ )
$X_e = RF * K * LS * C * PF * (907.18/4047)$	
$RF$	3.00E+02 Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor ( $yr^{-1}$ ) (Highest value from range listed in SLERA Protocol Table B-2-7)
$K$	3.60E-01 USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7 <sup>1</sup> )
$LS$	1.50E+00 USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7 <sup>2</sup> )
$C$	7.00E-01 USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7 <sup>3</sup> )
$PF$	1.00E+00 USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place)
	9.07E+02 Units conversion factor ( $kg/ton$ )
	4.05E+03 Units conversion factor ( $m^3/acre$ )
$SD$	<b>8.55E-02</b> Watershed sediment delivery ratio (unitless)
$SD = a * (A_L)^b$	
$a$	1.20E+00 Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>4</sup> )
$A_L$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$b$	1.25E-01 Empirical slope coefficient (unitless) (default value from Table B-2-8)

Notes:

<sup>1</sup> Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>2</sup> Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>3</sup> Watershed area estimated to be receiving COPC is between 10 and 100 square miles.

**Table B3-4. Toluene Water Body Concentration**

$C_{w\text{tot}} = L_T / [Vf_c * f_{w\text{c}} + k_{w\text{t}} * A_w * (d_{w\text{c}} + d_{w\text{b}})]$	
$C_{w\text{tot}}$	4.17E+14 Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_T$	1.12E+04 Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_c$	1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$f_{w\text{c}}$	6.86E-01 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$f_{w\text{b}} = [(1 + Kd_{w\text{c}} * \text{TSS} * 10^3) * d_{w\text{c}}/d_z] / [(1 + Kd_{w\text{c}} * \text{TSS} * 1 \times 10^3) * d_{w\text{c}}/d_z + (q_{w\text{b}} + Kd_{w\text{b}} * \text{BS}) * d_{w\text{b}}/d_z]$	
$f_{w\text{b}}$	3.14E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{w\text{c}}$	1.05E+01 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-185)
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L) (High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
	1.00E-06 Units conversion factor (kg/mg)
$d_{w\text{c}}$	4.05E-01 Depth of water column (m) <sup>3</sup>
$d_{w\text{b}}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{w\text{c}} + d_{w\text{b}}$ )
$\text{BS}$	1.00E+00 Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/m <sup>3</sup> ) (default value from SLERA Protocol Table B-2-10)
$q_{w\text{b}}$	6.00E-01 Bed sediment porosity ( $L_{\text{water}}/L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{w\text{b}}$	5.60E+00 Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-185)
$k_{w\text{t}}$	1.03E+10 Overall total water body COPC dissipation rate constant (yr <sup>-1</sup> )
$k_{w\text{t}} = f_{w\text{c}} * k_w + f_{w\text{b}} * k_b$	
$f_{w\text{c}}$	6.86E-01 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_w$	1.92E+03 Water column volatilization rate constant (yr <sup>-1</sup> )
$f_{w\text{b}}$	3.14E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_b$	3.28E+10 Benthic burial rate constant (yr <sup>-1</sup> )
$A_w$	5.98E+07 Water body surface area ( $\text{m}^2$ )
$k_v$	1.92E+03 Water column volatilization rate constant (yr <sup>-1</sup> )
$k_v = K_v / [d_z * (1 + Kd_{w\text{c}} * \text{TSS} * 10^3)]$	
$K_v$	8.38E+02 Overall COPC transfer rate coefficient (m/yr)
$d_{w\text{c}}$	4.05E-01 Depth of water column (m)
$d_{w\text{b}}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{w\text{c}} + d_{w\text{b}}$ )
$Kd_{w\text{c}}$	1.05E+01 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-185)
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L)
	1.00E-06 Units conversion factor (kg/mg)
$K_t$	8.38E+02 Overall COPC transfer rate coefficient (m/yr)
$K_t = \{K_v^{-1} + [K_d * H/(R * T_{w\text{k}})]^{-1}\}^{-1} * q^{(T_{w\text{k}} - 293)}$	
$K_d$	8.02E+02 Liquid-phase transfer coefficient (m/yr)
$K_g$	3.65E+04 Gas-phase transfer coefficient (m/yr)
$H$	6.13E-03 Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-185)
$R$	8.21E-05 Universal gas constant (atm-m <sup>3</sup> /mol-K)
$T_{w\text{k}}$	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
$q$	1.03E+00 Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_L$	8.02E+02 Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_L = \text{SORT}(10^{-1} * D_w * u / d_z) * 3.1536 \times 10^7$	
$D_w$	9.23E-06 Diffusivity of COPC in water (cm <sup>2</sup> /s) (SLERA Protocol Table A-2-185)
$u$	3.05E-01 Current velocity (m/s) <sup>4</sup>
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{w\text{c}} + d_{w\text{b}}$ )
	3.15E+07 Units conversion constant (s/yr)
$K_G$	3.65E+04 Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$k_b$	3.28E+10 Benthic burial rate constant (yr <sup>-1</sup> )
$k_b = [X_w * A_t * SD * 10^3 - Vf_c * \text{TSS} / (A_w * \text{TSS})] * [\text{TSS} * 10^3 / (\text{BS} * d_{w\text{b}})]$	
$X_w$	2.54E+01 Unit soil loss (kg/m <sup>2</sup> -yr)
$A_t$	1.51E+09 Total watershed area receiving COPC deposition ( $\text{m}^2$ )
$SD$	8.55E-02 Watershed sediment delivery ratio (unitless)
$Vf_c$	1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$\text{TSS}$	3.00E+02 Total suspended solids concentration (mg/L)
$A_w$	5.98E+07 Water body surface area ( $\text{m}^2$ )
$\text{BS}$	1.00E+00 Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/m <sup>3</sup> ) (default value from SLERA Protocol Table B-2-16)
$d_{w\text{b}}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup> Assume pH = 8.0 based on water quality data provided by EPA Region 5

<sup>2</sup> Values found for data from Mississippi River near St. Louis range from 50-350 mg/L, therefore used high end of SLERA default range.

<sup>3</sup> Based on minimum depth required by Corps of Engineers

<sup>4</sup> Current velocity ranges from 3-7 ft/s based on information from several sources.

**Table B3-5. Toluene Concentration in Water Column**

$C_{wctot} = f_{wc} * C_{wtot} * (d_{wc} + d_{bs}) / d_{wc}$		
<b><math>C_{wctot}</math></b>	<b><math>3.07E-14</math></b>	Total COPC concentration in water column (mg/L)
$f_{wc}$	6.86E-01	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{wtot}$	4.17E-14	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B3-6. Toluene Dissolved Phase Water Concentration**

$C_{dw} = C_{wctot} / (1 + Kd_{sw} * TSS * 10^{-6})$		
$C_{dw}$	<b>3.06E-14</b>	Dissolved phase water concentration (mg/L)
$C_{wctot}$	3.07E-14	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	1.05E+01	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-185)
TSS	3.00E+02	Total suspended solids concentration (mg/L)

**Table B3-7. Toluene Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{bs}} * C_{\text{wtot}} * [\text{Kd}_{\text{bs}} / (q_{\text{bs}} + \text{Kd}_{\text{bs}} * BS)] * [(d_{\text{wc}} + d_{\text{bs}}) / d_{\text{bs}}]$				
<b><math>C_{\text{sed}}</math></b>	<b>1.72E-13</b>	COPC concentration in bed sediment (mg/kg)		
<b><math>f_{\text{bs}}</math></b>	<b>3.14E-01</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)		
<b><math>C_{\text{wtot}}</math></b>	<b>4.17E-14</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)		
<b><math>\text{Kd}_{\text{bs}}</math></b>	<b>5.60E+00</b>	Bed sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-185)		
<b><math>q_{\text{bs}}</math></b>	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}} / L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)		
<b><math>BS</math></b>	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)		
<b><math>d_{\text{wc}}</math></b>	<b>4.05E-01</b>	Depth of water column (m)*		
<b><math>d_{\text{bs}}</math></b>	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)		

**Table B4-1. Benzo(a)anthracene Summary**

	Concentration from Project	Background Concentration <sup>1</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>2</sup>	Toxicity Reference Value <sup>3</sup>	Project Increase Percent of Background Concentration	Ecological Screening Quotient
Soil (mg/kg)	3.98E-08	1.60E+01	1.60E+01	5.21E+00	2.50E+01	0.00%	N/A
Water (mg/L)	5.56E-21	N/A	N/A	2.50E-05	2.70E-05	N/A	0.00
Sediment (mg/kg)	8.45E-18	N/A	N/A	1.08E-01	1.90E-02	N/A	0.00

Notes:

<sup>1</sup> Soil background concentration obtained from USGS survey of the area around Chicago, IL; Kay, R.T., et al. Concentrations of Polynuclear Aromatic Hydrocarbons and Inorganic Constituents in Ambient Surface Soils, Chicago, Illinois: 2001-2002. United States Geological Survey, 2003.

<sup>2</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/reg5crca/ca/guidance.htm>.

<sup>3</sup> U.S. EPA, Office of Solid Waste. Screening Level Ecological Risk Assessment Protocol for Hazardous Waste Combustion Facilities, Volume 1. EPA 530-D-99-001A. August 1999.

**Table B4-2. Benzo(a)anthracene Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$	
<b>Cs</b>	<b>3.98E-08</b> COPC concentration in soil (mg COPC/kg soil)
<b>tD</b>	<b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)
<b>Ds</b>	<b>1.48E-08</b> Deposition term (mg COPC/kg soil/yr)
$D_s = 100/(Z_s * BD) * [F_v(Dydv + Dywv) + (Dywp + Dydp) * (1 - F_v)]$	
	1.00E+02 Units conversion factor ( $m^2\text{-mg}/cm^2\text{-kg}$ )
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$	8.81E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-19)
$Dydv + Dywv$	5.00E-09 Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2\text{-yr}$ )
$Dywp + Dydp$	3.60E-10 Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2\text{-yr}$ )
<b>ks</b>	<b>3.72E-01</b> COPC soil loss constant due to all soil processes ( $yr^{-1}$ )
$ks = k_{sg} + k_{se} + k_{sr} + k_{sl} + k_{sv}$	
$k_{sg}$	3.72E-01 COPC loss constant due to biotic and abiotic degradation ( $yr^{-1}$ ) (SLERA Protocol Table A-2-19 <sup>1</sup> )
$k_{se}$	0.00E+00 COPC loss constant due to soil erosion ( $yr^{-1}$ ) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$	3.26E-04 COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sl}$	0.00E+00 COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sv}$	1.81E-05 COPC loss constant due to volatilization ( $yr^{-1}$ )
<b>ksr</b>	<b>3.26E-04</b> COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sr} = RO / (0_{sw} * Z_s) * [1/[1 + (Kd_s * BD/0_{sw})]]$	
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$0_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	2.60E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-19 <sup>2</sup> )
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b>ksl</b>	<b>0.00E+00</b> COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sl} = (P + I - RO - E_v) / \{0_{sw} * Z_s * [1.0 + (BD * Kd_s / 0_{sw})]\}$	
$P$	1.02E+02 Annual average precipitation (cm/yr) (NOAA)
$I$	0.00E+00 Average annual irrigation (cm/yr) (Baes Reference to SLERA Protocol Table B-1-5, Assumed due to low irrigation percentage in Illinois)
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$E_v$	7.62E+01 Average annual evapotranspiration (cm/yr)
$0_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Kd_s$	2.60E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-19 <sup>2</sup> )
<b>ksv</b>	<b>1.81E-05</b>
$k_{sv} = [3.1536 \times 10^7 * H / (Z_s * Kd_s * R * T_d * BD)] * [D_s / Z_s] * [1 - (BD/\rho_s) - 0_{sw}]$	
	3.15E+07 Units conversion factor (s/yr)
$H$	3.62E-06 Henry's Law constant ( $atm\text{-}m}^3/mol$ ) (SLERA Protocol Table A-2-19)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	2.60E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-19 <sup>2</sup> )
$R$	8.21E-05 Universal gas constant ( $atm\text{-}m}^3/mol\text{-K}$ )
$T_d$	2.98E+02 Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$\rho_s$	2.70E+00 Solids particle density ( $g/cm^3$ ) ( default value from SLERA Protocol Table B-1-6)
$D_s$	2.47E-02 Diffusivity of COPC in air ( $cm^2/s$ ) ( SLERA Protocol Table A-2-19)
$0_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

<sup>1</sup> Assume ND = 0.

<sup>2</sup> Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

**Table B4-3. Benzo(a)anthracene Load to Water Body**

$L_1 = L_{DwP} + L_{Dw} + L_{R1} + L_e + L_r + L_i$	
$L_T = 4.98E-01$	Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DwP}$	2.66E-01 Total (wet and dry) particle phase and wet vapor phase COPC direct deposition load to water body (g/yr)
$L_{DwP} = A_w * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
$A_w$	5.98E+07 Water body surface area ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$F_v$	8.81E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-19)
$Dwvp$	5.00E-09 Yearly average wet deposition from vapor phase from model (over water body) ( $g/m^2 \cdot yr$ )
$Dwdpp$	3.60E-10 Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$L_{Dw}$	0.00E+00 Vapor phase COPC diffusion (dry deposition) load to water body (g/yr) <sup>1</sup>
$L_{Dw} = (K_c * F_v * Cvp * 1.0 \times 10^{-6}) / (H(R * T_{ak}))$	
$K_c$	6.09E+00 Overall transfer rate coefficient ( $m/yr$ )
$F_v$	8.81E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-19)
$Cvp$	0.00E+00 Yearly average air concentration from vapor phase from model (over water body) ( $mg/m^3$ )
$H$	3.62E-06 Henry's Law constant ( $atm \cdot m^3/mol$ ) (SLERA Protocol Table A-2-19)
$R$	8.21E-05 Universal gas constant ( $atm \cdot m^3/mol \cdot K$ )
$T_{ak}$	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_{R1}$	9.71E-02 Runoff load from impervious sources (g/yr)
$L_{R1} = A_t * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
$F_v$	8.81E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-19)
$Dwvp$	5.00E-09 Yearly average wet deposition from vapor phase from model (over water body) ( $g/m^2 \cdot yr$ )
$Dwdpp$	3.60E-10 Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$A_t$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$L_R$	5.79E-03 Runoff load from pervious sources (g/yr)
$L_R = RO * (A_L - A_t) * [(Cs * BD) / (0_{ro} + Kd_s * BD)] * 0.01$	
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/hq/hq730/ch_k/k-regionsum.html">http://pubs.usgs.gov/hq/hq730/ch_k/k-regionsum.html</a> )
$A_L$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$A_t$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$Cs$	3.98E-08 COPC concentration in soil (mg/kg)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$\theta_{rw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$Kd_s$	2.60E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-19)
	1.00E-02 Units conversion factor ( $kg \cdot cm^3/mg \cdot m^3$ )
$L_E$	1.29E-01 Soil erosion load (g/yr)
$L_E = X_e * (A_L - A_t) * SD * ER * [(Cs * Kd_s * BD) / (0_{ro} + Kd_s * BD)] * 0.001$	
$X_e$	2.54E+01 Unit soil loss ( $kg/m^2 \cdot yr$ )
$A_L$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$A_t$	2.18E+07 Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$SD$	8.55E-02 Watershed sediment delivery ratio (unitless)
$ER$	1.00E+00 Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for Inorganic COPC's and 3 for Organic COPC's)
$Cs$	3.98E-08 COPC concentration in soil (mg/kg)
$Kd_s$	2.60E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-19)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
$\theta_{rw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
	1.00E-03 Units conversion factor ( $g/mg$ )
$L_I$	0.00E+00 Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
$X_e$	2.54E+01 Unit soil loss ( $kg/m^2 \cdot yr$ )
$X_e = RF * K * LS * C * PF * (907.18/4047)$	
$RF$	3.00E+02 Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor ( $yr^{-1}$ ) (Highest value from range listed in SLERA Protocol Table B-2-7)
$K$	3.60E-01 USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7) <sup>2</sup>
$LS$	1.50E+00 USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7)
$C$	7.00E-01 USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7)
$PF$	1.00E+00 USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place)
	9.07E+02 Units conversion factor (kg/ton)
	4.05E+03 Units conversion factor ( $m^3/acre$ )
$SD$	8.55E-02 Watershed sediment delivery ratio (unitless)
$SD = a * (A_L)^b$	
$a$	1.20E+00 Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>3</sup> )
$A_L$	1.51E+09 Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$b$	1.25E-01 Empirical slope coefficient (unitless) (default value from Table B-2-8)

Notes:

<sup>1</sup> Assume vapor phase COPC diffusion load to water body is zero for Benzo(a)anthracene.

<sup>2</sup> Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>3</sup> Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>4</sup> Watershed area estimated to be receiving COPC is between 10 and 100 square miles.

**Table B4-4. Benzo(a)anthracene Water Body Concentration**

$C_{\text{water}} = L_T / [Vf_t * f_{wc} + k_{wt} * A_w * (d_{wc} + d_{bs})]$
$C_{\text{water}}$ 5.87E-19 Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_T$ 4.98E-01 Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_t$ 1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$f_{wc}$ 8.82E-03 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$f_{wc} = [(1 + Kd_{ws} * \text{TSS} * 10^6) * d_{wc}/d_z] / [(1 + Kd_{ws} * \text{TSS} * 10^6) * d_{wc}/d_z + (0_{bs} + Kd_{bs} * BS) * d_{bs}/d_z]$
$f_{bs}$ 1 - $f_{wc}$
$f_{bs}$ 9.91E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{ws}$ 1.95E+04 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-19 <sup>1</sup> )
$\text{TSS}$ 3.00E+02 Total suspended solids concentration (mg/L) <sup>2</sup> (High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
1.00E-06 Units conversion factor (kg/mg)
$d_{wc}$ 4.05E-01 Depth of water column (m) <sup>3</sup>
$d_{bs}$ 3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$ 4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{wc} + d_{bs}$ )
$BS$ 1.00E+00 Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)
$0_{bs}$ 6.00E-01 Bed sediment porosity ( $L_{\text{water}}/L_{\text{subsurface}}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{bs}$ 1.04E+04 Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-19 <sup>1</sup> )
$k_{wt}$ 3.25E+10 Overall total water body COPC dissipation rate constant ( $\text{yr}^{-1}$ ) <sup>4</sup>
$k_{wt} = f_{wc} * k_v + f_{bs} * k_b$
$f_{wc}$ 8.82E-03 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_v$ 2.04E+00 Water column volatilization rate constant ( $\text{yr}^{-1}$ )
$f_{bs}$ 9.91E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_b$ 3.28E+10 Benthic burial rate constant ( $\text{yr}^{-1}$ )
$A_w$ 5.98E+07 Water body surface area ( $\text{m}^2$ )
$k_v$ 2.04E+00 Water column volatilization rate constant ( $\text{yr}^{-1}$ )
$k_v = K_v / [d_z * (1 + Kd_{ws} * \text{TSS} * 10^6)]$
$K_v$ 6.09E+00 Overall COPC transfer rate coefficient (m/yr)
$d_{wc}$ 4.05E-01 Depth of water column (m)
$d_{bs}$ 3.00E-02 Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$ 4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{wc} + d_{bs}$ )
$Kd_{ws}$ 1.95E+04 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-19)
$\text{TSS}$ 3.00E+02 Total suspended solids concentration (mg/L)
1.00E-06 Units conversion factor (kg/mg)
$K_v$ 6.09E+00 Overall COPC transfer rate coefficient (m/yr)
$K_v = (K_L^{-1} + [K_0 * H/(R * T_{wk})]^{-1})^{-1} * q^{(T_{wk} - 293)}$
$K_L$ 6.58E+02 Liquid-phase transfer coefficient (m/yr)
$K_G$ 3.65E+04 Gas-phase transfer coefficient (m/yr)
$H$ 3.62E-06 Henry's Law constant (atm· $\text{m}^3/\text{mol}$ ) (SLERA Protocol Table A-2-19)
$R$ 8.21E-05 Universal gas constant (atm· $\text{m}^3/\text{mol}\cdot\text{K}$ )
$T_{wk}$ 2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
$q$ 1.03E+00 Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_L$ 6.58E+02 Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_L = \text{SQRT} (10^4 * D_w * u / d_z) * 3.1536 \times 10^7$
$D_w$ 6.21E-06 Diffusivity of COPC in water ( $\text{cm}^2/\text{s}$ ) (SLERA Protocol Table A-2-19)
$u$ 3.05E-01 Current velocity ( $\text{m/s}$ ) <sup>4</sup>
$d_z$ 4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{wc} + d_{bs}$ )
3.15E+07 Units conversion constant ( $\text{s}^2/\text{yr}$ )
$K_G$ 3.65E+04 Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$k_b$ 3.28E+10 Benthic burial rate constant ( $\text{yr}^{-1}$ )
$k_b = [X_e * A_L * SD * 10^3 - Vf_t * \text{TSS} / (A_w * \text{TSS})] * [\text{TSS} * 10^6 / (BS * d_{bs})]$
$X_e$ 2.54E+01 Unit soil loss ( $\text{kg/m}^2\cdot\text{yr}$ )
$A_L$ 1.51E+09 Total watershed area receiving COPC deposition ( $\text{m}^2$ )
$SD$ 8.55E-02 Watershed sediment delivery ratio (unitless)
$Vf_t$ 1.32E+08 Average volumetric flow rate through water body ( $\text{m}^3/\text{yr}$ )
$\text{TSS}$ 3.00E+02 Total suspended solids concentration (mg/L)
$A_w$ 5.98E+07 Water body surface area ( $\text{m}^2$ )
$BS$ 1.00E+00 Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-16)
$d_{bs}$ 3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup> Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

<sup>2</sup> No data available for location of deposition, therefore used high end of SLERA default range.

<sup>3</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

<sup>4</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

**Table B4-5. Benzo(a)anthracene Concentration in Water Column**

$C_{wctot} = f_{wc} * C_{wtot} * (d_{wc} + d_{bs}) / d_{wc}$		
<b>5.56E-21</b>	Total COPC concentration in water column (mg/L)	
$f_{wc}$	8.82E-03	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{wtot}$	5.87E-19	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B4-6. Benzo(a)anthracene Dissolved Phase Water Concentration**

$C_{dw} = C_{wetot} / (1 + Kd_{sw} * TSS * 10^{-6})$		
$C_{dw}$	<b>8.12E-22</b>	Dissolved phase water concentration (mg/L)
$C_{wetot}$	5.56E-21	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	1.95E+04	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-19)
TSS	3.00E+02	Total suspended solids concentration (mg/L)

**Table B4-7. Benzo(a)anthracene Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{bs}} * C_{\text{wtotal}} * [\text{Kd}_{\text{bs}} / (\theta_{\text{bs}} + \text{Kd}_{\text{bs}} * \text{BS})] * [(d_{\text{wc}} + d_{\text{bs}}) / d_{\text{bs}}]$				
<b><math>C_{\text{sed}}</math></b>	<b>8.45E-18</b>	COPC concentration in bed sediment (mg/kg)		
<b><math>f_{\text{bs}}</math></b>	<b>9.91E-01</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)		
<b><math>C_{\text{wtotal}}</math></b>	<b>5.87E-19</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)		
<b><math>\text{Kd}_{\text{bs}}</math></b>	<b>1.04E+04</b>	Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-19)		
<b><math>\theta_{\text{bs}}</math></b>	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}} / L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)		
<b>BS</b>	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)		
<b><math>d_{\text{wc}}</math></b>	<b>4.05E-01</b>	Depth of water column (m)*		
<b><math>d_{\text{bs}}</math></b>	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)		

**Table B5-1. Benzo(a)pyrene Summary**

	Concentration from Project	Background Concentration <sup>1,2</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>3</sup>	Toxicity Reference Value <sup>4</sup>	Project Increase Percent of Background Concentration	Ecological Screening Quotient
Soil (mg/kg)	9.47E-09	1.70E+01	1.70E+01	1.52E+00	2.50E+01	0.00%	N/A
Water (mg/L)	1.42E-21	2.00E-05	2.00E-05	1.40E-05	1.40E-05	0.00%	N/A
Sediment (mg/kg)	2.41E-18	N/A	N/A	1.50E-01	8.40E-02	N/A	0.00

Notes:

<sup>1</sup> Soil background concentration obtained from USGS survey of the area around Chicago, IL. Kay, R.T., et al. Concentrations of Polynuclear Aromatic Hydrocarbons and Inorganic Constituents in Ambient Surface Soils, Chicago, Illinois: 2001-2002. United States Geological Survey, 2003.

<sup>2</sup> Water background concentration assumed to be the average concentration from water samples in or near Jefferson County, obtained from the EPA on 01/19/11 via J. Schewe of Falcon Engineering.

<sup>3</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/reg5rcra/ca/guidance.htm>.

<sup>4</sup> U.S. EPA, Office of Solid Waste. Screening Level Ecological Risk Assessment Protocol for Hazardous Waste Combustion Facilities, Volume 1. EPA 530-D-99-001A. August 1999.

**Table B5-2. Benzo(a)pyrene Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$	
<b><math>C_s</math></b>	<b>9.47E-09</b> COPC concentration in soil (mg COPC/kg soil)
<b><math>tD</math></b>	<b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)
<b><math>D_s</math></b>	<b>4.52E-09</b> Deposition term (mg COPC/kg soil/yr)
$D_s = 100/(Z_s * BD) * [F_v (Dydv + Dywv) + (Dywp + Dydp) * (1 - F_v)]$	
	1.00E+02 Units conversion factor ( $m^2\text{-mg/cm}^2\text{-kg}$ )
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$	2.65E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-20)
$Dydv + Dywv$	1.04E-09 Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2\text{-yr}$ )
$Dywp + Dydp$	1.47E-09 Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2\text{-yr}$ )
<b><math>k_s</math></b>	<b>4.77E-01</b> COPC soil loss constant due to all soil processes ( $yr^{-1}$ )
$k_s = k_{sg} + k_{se} + k_{sr} + k_{sl} + k_{sv}$	
$k_{sg}$	4.77E-01 COPC loss constant due to biotic and abiotic degradation ( $yr^{-1}$ ) (SLERA Protocol Table A-2-20 <sup>1</sup> )
$k_{se}$	0.00E+00 COPC loss constant due to soil erosion ( $yr^{-1}$ ) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$	8.74E-05 COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sl}$	0.00E+00 COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sv}$	9.88E-07 COPC loss constant due to volatilization ( $yr^{-1}$ )
<b><math>k_{sr}</math></b>	<b>8.74E-05</b> COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sr} = RO / (θ_{sw} * Z_s) * [1/[1 + (Kd_s * BD/θ_{sw})]]$	
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$θ_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	9.69E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-20 <sup>2</sup> )
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b><math>k_{sl}</math></b>	<b>0.00E+00</b> COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sl} = (P + I - RO - E_v) / [θ_{sw} * Z_s * [1.0 + (BD * Kd_s / θ_{sw})]]$	
$P$	1.02E+02 Annual average precipitation (cm/yr) (NOAA)
$I$	0.00E+00 Average annual irrigation (cm/yr) (Baes Reference to SLERA Protocol Table B-1-5, Assumed due to low irrigation percentage in Illinois)
$RO$	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$E_v$	7.62E+01 Average annual evapotranspiration (cm/yr)
$θ_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Kd_s$	9.69E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-20 <sup>2</sup> )
<b><math>k_{sv}</math></b>	<b>9.88E-07</b>
$k_{sv} = [3.1536 \times 10^7 * H / (Z_s * Kd_s * R * T_a * BD)] * [D_a / Z_s] * [1 - (BD/p_s) - θ_{sw}]$	
	3.15E+07 Units conversion factor (s/yr)
$H$	8.36E-07 Henry's Law constant ( $atm\cdot m^3/mol$ ) (SLERA Protocol Table A-2-20)
$Z_s$	2.00E+01 Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$	9.69E+03 Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-20 <sup>2</sup> )
$R$	8.21E-05 Universal gas constant ( $atm\cdot m^3/mol\cdot K$ )
$T_a$	2.98E+02 Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
$BD$	1.50E+00 Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$p_s$	2.70E+00 Solids particle density ( $g/cm^3$ ) ( default value from SLERA Protocol Table B-1-6)
$D_a$	2.18E-02 Diffusivity of COPC in air ( $cm^2/s$ ) ( SLERA Protocol Table A-2-20)
$θ_{sw}$	2.00E-01 Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

<sup>1</sup> Assume ND = 0.

<sup>2</sup> Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

**Table B5-3. Benzo(a)pyrene Load to Water Body**

$L_1 = L_{DWP} + L_{VAP} + L_{RI} + L_R + L_E + L_I$	
$L_T = 1.42E-01$	Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DWP}$	<b>8.11E-02</b> Total (wet and dry) particle phase and wet vapor phase COPC direct deposition load to water body (g/yr)
$L_{DWP} = A_w * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
$A_w$	5.98E+07 Water body surface area ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$F_v$	2.65E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-20)
$Dwvp$	1.04E-09 Yearly average wet deposition from vapor phase from model (over water body)( $g/m^2 \cdot yr$ )
$Dwdpp$	1.47E-09 Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$L_{DWP}$	<b>0.000E+00</b> Vapor phase COPC diffusion (dry deposition) load to water body (g/yr)
$L_{DWP} = (K_e * F_v * Cvp * 1.0 \times 10^{-6}) / (H/R^*T_{ab})$	
$K_e$	<b>1.42E+00</b> Overall transfer rate coefficient ( $m/yr$ )
$F_v$	<b>2.65E-01</b> Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-20)
$Cvp$	<b>0.000E+00</b> Yearly average air concentration from vapor phase from model (over water body) ( $mg/m^3$ )
$H$	<b>8.36E-07</b> Henry's Law constant ( $atm \cdot m^3/mol$ ) (SLERA Protocol Table A-2-20)
$R$	<b>8.31E-05</b> Universal gas constant ( $atm \cdot m^3/mol \cdot K$ )
$T_{ab}$	<b>2.98E+02</b> Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_{RI}$	<b>2.96E-02</b> Runoff load from impervious sources (g/yr)
$L_{RI} = A_i * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
$F_v$	<b>2.65E-01</b> Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-20)
$Dwvp$	<b>1.04E-09</b> Yearly average wet deposition from vapor phase from model (over water body) ( $g/m^2 \cdot yr$ )
$Dwdpp$	<b>1.47E-09</b> Yearly average total (wet and dry) deposition from particle phase from model (over water body) ( $g/m^2 \cdot yr$ )
$A_i$	<b>2.18E+07</b> Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$L_R$	<b>3.70E-04</b> Runoff load from pervious sources (g/yr)
$L_R = RO * (A_i - A_l) * [(Cs * BD) / (\theta_{so} + Kd * BD)] * 0.01$	
$RO$	<b>2.54E+01</b> Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/har/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/har/ha730/ch_k/k-regionalsum.html</a> )
$A_L$	<b>1.51E+09</b> Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$A_l$	<b>2.18E+07</b> Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$Cs$	<b>9.47E-09</b> COPC concentration in soil (mg/kg)
$BD$	<b>1.50E+00</b> Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$\theta_{so}$	<b>2.00E-01</b> Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-5)
$Kd$	<b>9.69E+03</b> Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-20)
	<b>1.00E-02</b> Units conversion factor ( $kg \cdot cm^2/m^2 \cdot m^-3$ )
$L_E$	<b>3.07E-02</b> Soil erosion load (g/yr)
$L_E = X_e * (A_l - A_i) * SD * ER * [(Cs * Kd * BD) / (\theta_{so} + Kd * BD)] * 0.001$	
$X_e$	<b>2.54E+01</b> Unit soil loss ( $kg/m^2 \cdot yr$ )
$A_L$	<b>1.51E+09</b> Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$A_i$	<b>2.18E+07</b> Impervious watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$SD$	<b>8.55E-02</b> Watershed sediment delivery ratio (unitless)
$ER$	<b>1.00E+00</b> Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for Inorganic COPC's and 3 for Organic COPC's)
$Cs$	<b>9.47E-09</b> COPC concentration in soil (mg/kg)
$Kd$	<b>9.69E+03</b> Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-20)
$BD$	<b>1.50E+00</b> Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
$\theta_{so}$	<b>2.00E-01</b> Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-2-6)
	<b>1.00E-03</b> Units conversion factor ( $g/mg$ )
$L_I$	<b>0.000E+00</b> Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
$X_e$	<b>2.54E+01</b> Unit soil loss ( $kg/m^2 \cdot yr$ )
$X_e = RF * K * LS * C * PF * (907.18/4047)$	
$RF$	<b>3.00E+02</b> Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor ( $yr^{-1}$ ) (Highest value from range listed in SLERA Protocol Table B-2-7)
$K$	<b>3.60E-01</b> USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7 <sup>2</sup> )
$LS$	<b>1.50E+00</b> USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7 <sup>2</sup> )
$C$	<b>7.00E-01</b> USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7 <sup>2</sup> )
$PF$	<b>1.00E+00</b> USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place)
	<b>9.07E+02</b> Units conversion factor (kg/ton)
	<b>4.05E-03</b> Units conversion factor ( $m^3/acre$ )
$SD$	<b>8.55E-02</b> Watershed sediment delivery ratio (unitless)
$SD = a * (A_l)^b$	
$a$	<b>1.20E+00</b> Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>3</sup> )
$A_L$	<b>1.51E+09</b> Total watershed area receiving COPC deposition ( $m^2$ ) (Illinois Department of Agriculture. 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$b$	<b>1.25E-01</b> Empirical slope coefficient (unitless) (default value from Table B-2-8)

Notes:

<sup>1</sup> Assume vapor phase COPC diffusion load to water body is zero for Benzo(a)pyrene.

<sup>2</sup> Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>3</sup> Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>4</sup> Watershed area estimated to be receiving COPC is between 10 and 100 square miles.

**Table B5-4. Benzo(a)pyrene Water Body Concentration**

$C_{w\text{tot}} = L_T / [Vf_w * f_{wc} + k_{wt} * A_w * (d_{wc} + d_{bs})]$	
$C_{w\text{tot}}$	<b>1.67E-19</b> Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_T$	<b>1.42E-01</b> Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_w$	<b>1.32E+08</b> Average volumetric flow rate through water body (m <sup>3</sup> /yr)
$f_{wc}$	<b>7.90E-03</b> Fraction of total water body COPC concentration that occurs in the water column (unitless)
$f_{wc}$	$= [(1 + Kd_{sw} * TSS * 10^{-6}) * d_{wc}/d_z] / [(1 + Kd_{sw} * TSS * 1 \times 10^{-6}) * d_{wc}/d_z + (b_{bs} + Kd_{bs} * BS) * d_{bs}/d_z]$
$f_{wc}$	$= 1 - f_{bs}$
$f_{bs}$	<b>9.92E-01</b> Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{sw}$	<b>7.27E+04</b> Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-20 <sup>1</sup> )
TSS	<b>3.00E+02</b> Total suspended solids concentration (mg/L)(High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
	<b>1.00E-06</b> Units conversion factor (kg/mg)
$d_{wc}$	<b>4.05E-01</b> Depth of water column (m) <sup>3</sup>
$d_{bs}$	<b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$	<b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{wc} + d_{bs}$ )
BS	<b>1.00E+00</b> Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)
$b_{bs}$	<b>6.00E-01</b> Bed sediment porosity ( $L_{water}/L_{sediment}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{bs}$	<b>3.87E+04</b> Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-20 <sup>1</sup> )
$k_{wt}$	<b>3.26E+10</b> Overall total water body COPC dissipation rate constant (yr <sup>-1</sup> ) <sup>4</sup>
$k_{wt}$	$= f_{wc} * k_w + f_{bs} * k_b$
$f_{wc}$	<b>7.90E-03</b> Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_w$	<b>1.43E-01</b> Water column volatilization rate constant (yr <sup>-1</sup> )
$f_{bs}$	<b>9.92E-01</b> Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_b$	<b>3.28E+10</b> Benthic burial rate constant (yr <sup>-1</sup> )
$A_w$	<b>5.98E+07</b> Water body surface area (m <sup>2</sup> )
$k_v$	<b>1.43E-01</b> Water column volatilization rate constant (yr <sup>-1</sup> )
$k_v$	$= K_v / [d_z * (1 + Kd_{sw} * TSS * 10^{-6})]$
$K_v$	<b>1.42E+00</b> Overall COPC transfer rate coefficient (m/yr)
$d_{wc}$	<b>4.05E-01</b> Depth of water column (m)
$d_{bs}$	<b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$	<b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{wc} + d_{bs}$ )
$Kd_{sw}$	<b>7.27E+04</b> Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-20)
TSS	<b>3.00E+02</b> Total suspended solids concentration (mg/L)
	<b>1.00E-06</b> Units conversion factor (kg/mg)
$K_t$	<b>1.42E+00</b> Overall COPC transfer rate coefficient (m/yr)
$K_t$	$= [K_l^{-1} + (K_G * H/(R * T_{wk}))^{-1}]^{-1} * q^{(T_{wk} - 29)}$
$K_l$	<b>6.38E+02</b> Liquid-phase transfer coefficient (m/yr)
$K_G$	<b>3.65E+04</b> Gas-phase transfer coefficient (m/yr)
H	<b>8.36E-07</b> Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-20)
R	<b>8.21E-05</b> Universal gas constant (atm-m <sup>3</sup> /mol-K)
$T_{wk}$	<b>2.98E+02</b> Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
q	<b>1.03E+00</b> Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_l$	<b>6.38E+02</b> Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_l$	$= \text{SQRT} (10^4 * D_w * u / d_z) * 3.1536 \times 10^7$
$D_w$	<b>5.85E-06</b> Diffusivity of COPC in water (cm <sup>2</sup> /s) (SLERA Protocol Table A-2-20)
u	<b>3.05E-01</b> Current velocity (m/s) <sup>4</sup>
$d_z$	<b>4.35E-01</b> Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{wc} + d_{bs}$ )
	<b>3.15E+07</b> Units conversion constant (s/ $\sqrt{\text{m}}$ )
$K_G$	<b>3.65E+04</b> Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$k_b$	<b>3.28E+10</b> Benthic burial rate constant (yr <sup>-1</sup> )
$k_b$	$= [X_c * A_L * SD * 10^3 - Vf_w * TSS / (A_w * TSS)] * [TSS * 10^{-6} / (BS * d_{sol})]$
$X_c$	<b>2.54E+01</b> Unit soil loss (kg/m <sup>2</sup> -yr)
$A_L$	<b>1.51E+09</b> Total watershed area receiving COPC deposition (m <sup>2</sup> )
SD	<b>8.55E-02</b> Watershed sediment delivery ratio (unitless)
$Vf_w$	<b>1.32E+08</b> Average volumetric flow rate through water body (m <sup>3</sup> /yr)
TSS	<b>3.00E+02</b> Total suspended solids concentration (mg/L)
$A_w$	<b>5.98E+07</b> Water body surface area (m <sup>2</sup> )
BS	<b>1.00E+00</b> Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-16)
$d_{bs}$	<b>3.00E-02</b> Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup> Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

<sup>2</sup> No data available for location of deposition, therefore used high end of SLERA default range.

<sup>3</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

<sup>4</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

**Table B5-5. Benzo(a)pyrene Concentration in Water Column**

$C_{wctot} = f_{wc} * C_{wtot} * (d_{wc} + d_{bs}) / d_{wc}$		
<b>1.42E-21</b> Total COPC concentration in water column (mg/L)		
$f_{wc}$	7.90E-03	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{wtot}$	1.67E-19	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B5-6. Benzo(a)pyrene Dissolved Phase Water Concentration**

$C_{dw} = C_{wetot} / (1 + Kd_{sw} * TSS * 10^{-6})$		
$C_{dw}$	<b>6.22E-23</b>	Dissolved phase water concentration (mg/L)
$C_{wetot}$	1.42E-21	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	7.27E+04	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-20)
TSS	3.00E+02	Total suspended solids concentration (mg/L)

**Table B5-7. Benzo(a)pyrene Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{bs}} * C_{\text{wtot}} * [Kd_{\text{bs}} / (\theta_{\text{bs}} + Kd_{\text{bs}} * BS)] * [(d_{\text{wc}} + d_{\text{bs}})/d_{\text{bs}}]$			
$C_{\text{sed}}$	<b>2.41E-18</b>	COPC concentration in bed sediment (mg/kg)	
$f_{\text{bs}}$	<b>9.92E-01</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)	
$C_{\text{wtot}}$	<b>1.67E-19</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)	
$Kd_{\text{bs}}$	<b>3.87E+04</b>	Bed sediment/pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-20)	
$\theta_{\text{bs}}$	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}}/L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)	
$BS$	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g}/\text{cm}^3$ ) (equivalent to $\text{kg}/\text{m}^3$ ) (default value from SLERA Protocol Table B-2-10)	
$d_{\text{wc}}$	<b>4.05E-01</b>	Depth of water column (m)*	
$d_{\text{bs}}$	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)	

**Table B6-1. Benzo(b)fluoranthene Summary**

	Concentration from Project	Background Concentration <sup>1</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>2</sup>	Toxicity Reference Value <sup>3</sup>	Total Concentration Percent of ESL	Ecological Screening Quotient
Soil (mg/kg)	3.61E-09	1.80E-01	1.80E+01	5.98E+01	2.50E+01	30.10%	N/A
Water (mg/L)	4.89E-22	N/A	N/A	9.07E-03	2.70E-05	N/A	0.00
Sediment (mg/kg)	8.24E-19	N/A	N/A	1.04E+01	3.70E-02	N/A	0.00

Notes:

<sup>1</sup> Soil background concentration obtained from USGS survey of the area around Chicago, IL. Kay, R.T., et al, Concentrations of Polynuclear Aromatic Hydrocarbons and Inorganic Constituents in Ambient Surface Soils, Chicago, Illinois: 2001-2002. United States Geological Survey, 2003.

<sup>2</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/region5/crra/ca/guidance.htm>.

<sup>3</sup> U.S. EPA, Office of Solid Waste, Screening Level Ecological Risk Assessment Protocol for Hazardous Waste Combustion Facilities, Volume 1: EPA 530-D-99-001A, August 1999.

**Table B6-2. Benzo(b)fluoranthene Soil Concentration**

$C_s = D_s * [1 - \exp(-k_s * tD)] / k_s$
<b>Cs</b> <b>3.61E-09</b> COPC concentration in soil (mg COPC/kg soil)
<b>tD</b> <b>1.00E+02</b> Time period over which deposition occurs (yr) (default value from SLERA Protocol Table B-1-1)
<b>Ds</b> <b>1.50E-09</b> Deposition term (mg COPC/kg soil/yr)
$D_s = 100/(Z_s * BD) * [F_v(Dydv + Dywv) + (Dywp + Dydp) * (1 - F_v)]$
1.00E+02    Units conversion factor ( $m^2\text{-mg/cm}^2\text{-kg}$ )
$Z_s$ 2.00E+01    Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-1, use 1 cm for untilled and 20 cm tilled soil)
$BD$ 1.50E+00    Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-1)
$F_v$ 8.22E-01    Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-21)
$Dydv + Dywv$ 4.30E-10    Maximum yearly average total (wet+dry) deposition from vapor phase from model ( $g/m^2\text{-yr}$ )
$Dywp + Dydp$ 5.40E-10    Maximum yearly average total (wet+dry) deposition from particle phase from model ( $g/m^2\text{-yr}$ )
<b>ks</b> <b>4.15E-01</b> COPC soil loss constant due to all soil processes ( $yr^{-1}$ )
$k_s = k_{sg} + k_{sc} + k_{sr} + k_{sl} + k_{sv}$
$k_{sg}$ 4.15E-01    COPC loss constant due to biotic and abiotic degradation ( $yr^{-1}$ ) (SLERA Protocol Table A-2-21 <sup>1</sup> )
$k_{sc}$ 0.00E+00    COPC loss constant due to soil erosion ( $yr^{-1}$ ) (default value from SLERA Protocol Table B-1-2)
$k_{sr}$ 1.01E-04    COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sl}$ 0.00E+00    COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sv}$ 8.86E-06    COPC loss constant due to volatilization ( $yr^{-1}$ )
<b>ksr</b> <b>1.01E-04</b> COPC loss constant due to surface runoff ( $yr^{-1}$ )
$k_{sr} = RO / (\theta_{sw} * Z_s) * \{1/[1 + (Kd_s * BD/\theta_{sw})]\}$
$RO$ 2.54E+01    Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$\theta_{sw}$ 2.00E-01    Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
$Z_s$ 2.00E+01    Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-4, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$ 8.36E+03    Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-21 <sup>2</sup> )
$BD$ 1.50E+00    Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-4)
<b>ksl</b> <b>0.00E+00</b> COPC loss constant due to leaching ( $yr^{-1}$ )
$k_{sl} = (P + I - RO - E_v) / \{\theta_{sw} * Z_s * [1.0 + (BD * Kd_s / \theta_{sw})]\}$
$P$ 1.02E+02    Annual average precipitation (cm/yr) (NOAA)
$I$ 0.00E+00    Average annual irrigation (cm/yr) (Baes Reference to SLERA Protocol Table B-1-5, Assumed due to low irrigation percentage in Illinois)
$RO$ 2.54E+01    Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_k/k-regionalsum.html</a> )
$E_v$ 7.62E+01    Average annual evapotranspiration (cm/yr)
$\theta_{sw}$ 2.00E-01    Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Z_s$ 2.00E+01    Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-5, use 1 cm for untilled and 20 cm tilled soil)
$BD$ 1.50E+00    Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-5)
$Kd_s$ 8.36E+03    Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-21 <sup>2</sup> )
<b>ksv</b> <b>8.86E-06</b>
$k_{sv} = [3.1536 \times 10^{-7} * H / (Z_s * Kd_s * R * T_g * BD)] * [D_s / Z_s] * [1 - (BD/\rho_s) - \theta_{sw}]$
3.15E+07    Units conversion factor (s/yr)
$H$ 6.18E-06    Henry's Law constant ( $atm\cdot m^3/mol$ ) (SLERA Protocol Table A-2-21)
$Z_s$ 2.00E+01    Soil mixing zone depth (cm) (per SLERA Protocol Table B-1-6, use 1 cm for untilled and 20 cm tilled soil)
$Kd_s$ 8.36E+03    Soil-water partition coefficient ( $cm^3/g$ ) (SLERA Protocol Table A-2-21 <sup>2</sup> )
$R$ 8.21E-05    Universal gas constant ( $atm\cdot m^3/mol\cdot K$ )
$T_g$ 2.98E+02    Ambient air temperature (K) (default value from SLERA Protocol Table B-1-6)
$BD$ 1.50E+00    Soil bulk density ( $g/cm^3$ ) (default value from SLERA Protocol Table B-1-6)
$\rho_s$ 2.70E+00    Solids particle density ( $g/cm^3$ ) ( default value from SLERA Protocol Table B-1-6)
$D_s$ 2.28E-02    Diffusivity of COPC in air ( $cm^2/s$ ) ( SLERA Protocol Table A-2-21)
$\theta_{sw}$ 2.00E-01    Soil volumetric water content ( $mL/cm^3$ ) (default value from SLERA Protocol Table B-1-6)

<sup>1</sup>Assume ND = 0.

<sup>2</sup>Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

**Table B6-3. Benzo(b)fluoranthene Load to Water Body**

$L_T = L_{DWP} + L_{DP} + L_{E} + L_R + L_I$	
$L_T = 4.86E-02$	Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$L_{DP} = A_w * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
A <sub>w</sub>	5.98E+07 Water body surface area (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
F <sub>v</sub>	8.22E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-21)
Dwvp	4.30E-10 Yearly average wet deposition from vapor phase from model (over water body)(g/m <sup>2</sup> -yr)
Dwdpp	5.40E-10 Yearly average total (wet and dry) deposition from particle phase from model (over water body) (g/m <sup>2</sup> -yr)
$L_{DP} = 2.69E-02$	Total (wet and dry) particle phase and w <sub>v</sub> vapor phase COPC direct deposition load to water body (g/yr)
$L_{E} = (K_e * F_v * Cvp * 1.0 \times 10^{-6}) / (H/R*T_{ab})$	
K <sub>e</sub>	1.03E-01 Overall transfer rate coefficient (m/yr)
F <sub>v</sub>	8.22E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-21)
Cvp	0.00E+00 Yearly average air concentration from vapor phase from model (over water body) (mg/m <sup>3</sup> )
H	6.18E-06 Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-21)
R	8.21E-05 Universal gas constant (atm-m <sup>3</sup> /mol-K)
T <sub>ab</sub>	2.98E-02 Water body temperature (K) (default value from SLERA Protocol Table B-2-3)
$L_R = 9.82E-03$	Runoff load from impervious sources (g/yr)
$L_R = A_i * [F_v * Dwvp + (1-F_v) * Dwdpp]$	
F <sub>v</sub>	8.22E-01 Fraction of COPC air concentration in vapor phase (SLERA Protocol Table A-2-21)
Dwvp	4.30E-10 Yearly average wet deposition from vapor phase from model (over water body)(g/m <sup>2</sup> -yr)
Dwdpp	5.40E-10 Yearly average total (wet and dry) deposition from particle phase from model (over water body) (g/m <sup>2</sup> -yr)
A <sub>i</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
$L_R = 1.63E-04$	Runoff load from pervious sources (g/yr)
$L_R = RO * (A_i - A_p) * [(Cs * BD) / (theta_p + Kd * BD)] * 0.01$	
RO	2.54E+01 Average annual surface runoff (cm/yr) (USGS Groundwater Atlas of the United States: Illinois, Indiana, Kentucky, Ohio, Tennessee available at <a href="http://pubs.usgs.gov/ha/ha730/ch_4/k-regionalsum.html">http://pubs.usgs.gov/ha/ha730/ch_4/k-regionalsum.html</a> )
A <sub>i</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
A <sub>p</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
Cs	3.61E-09 COPC concentration in soil (mg/kg)
BD	1.50E+00 Soil bulk density (g/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-5)
θ <sub>soil</sub>	2.00E-01 Soil volumetric water content (mL/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-5)
Kd	8.36E+03 Soil-water partition coefficient (cm <sup>3</sup> /g) (SLERA Protocol Table A-2-21)
	1.00E-02 Units conversion factor (kg-cm <sup>3</sup> /mg-m <sup>3</sup> )
$L_E = 1.17E-02$	Soil erosion load (g/yr)
$L_E = X_e * (A_i - A_p) * SD * ER * [(Cs * Kd * BD) / (theta_p + Kd * BD)] * 0.001$	
X <sub>e</sub>	2.54E+01 Unit soil loss (kg/m <sup>2</sup> -yr)
A <sub>i</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
A <sub>p</sub>	2.18E+07 Impervious watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
SD	8.55E-02 Watershed sediment delivery ratio (unitless)
ER	1.00E+00 Soil enrichment ratio (unitless) (Per SLERA Protocol Table B-2-6, value is 1 for inorganic COPC's and 3 for Organic COPC's)
Cs	3.61E-09 COPC concentration in soil (mg/kg)
Kd	8.36E+03 Soil-water partition coefficient (cm <sup>3</sup> /g) (SLERA Protocol Table A-2-21)
BD	1.50E+00 Soil bulk density (g/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-6)
θ <sub>soil</sub>	2.00E-01 Soil volumetric water content (mL/cm <sup>3</sup> ) (default value from SLERA Protocol Table B-2-6)
	1.00E-03 Units conversion factor (g/mg)
$L_I = 0.00E+00$	Internal transfer load (g/yr) (default value from SLERA Protocol Section 3.11.2.1)
X <sub>e</sub>	2.54E+01 Unit soil loss (kg/m <sup>2</sup> -yr)
X <sub>e</sub> = RF * K * LS * C * PF * (907.18/4047)	
RF	3.00E+02 Universal Soil Loss Equation (USLE) rainfall (or erosivity) factor (yr <sup>-1</sup> ) (Highest value from range listed in SLERA Protocol Table B-2-7)
K	3.60E-01 USLE erodibility factor (ton/acre) (Default value from SLERA Protocol Table B-2-7 <sup>2</sup> )
LS	1.50E+00 USLE length-slope factor (unitless) (default value for representative watershed from SLERA Protocol Table B-2-7 <sup>3</sup> )
C	7.00E-01 USLE cover management factor (unitless) (Value based on agricultural row cropland from SLERA Protocol Table B-2-7)
PF	1.00E+00 USLE supporting practice factor (unitless) (Assumes no erosion control measures are in place)
	9.07E+02 Units conversion factor (kg/ton)
	4.05E+03 Units conversion factor (m <sup>2</sup> /acre)
SD	8.55E-02 Watershed sediment delivery ratio (unitless)
SD = a * (A <sub>i</sub> ) <sup>b</sup>	
a	1.20E+00 Empirical intercept coefficient (unitless) (Value from Table B-2-8 based on watershed area <sup>4</sup> )
A <sub>i</sub>	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> ) (Illinois Department of Agriculture, 2007. Land Cover of Illinois. Available online at <a href="http://www.agr.state.il.us/gis/landcover99-00.html#class">http://www.agr.state.il.us/gis/landcover99-00.html#class</a> accessed [12/06/2010])
b	1.25E-01 Empirical slope coefficient (unitless) (default value from Table B-2-8)

Notes:

<sup>1</sup> Assume vapor phase COPC diffusion load to water body is zero for Benzo(b)fluoranthene.

<sup>2</sup> Based on other available data, silty loam soils such as those found in this watershed have K values ranging from 0.25 - 0.4.

<sup>3</sup> Majority of watershed area has slopes 0% - 10%, therefore default value of 1.5 LS is used.

<sup>4</sup> Watershed area estimated to be receiving COPC I between 10 and 100 square miles.

**Table B6-4. Benzo(b)fluoranthene Water Body Concentration**

$C_{\text{water}} = L_T / [Vf_w * f_{wc} + k_{wt} * A_w * (d_{wc} + d_{bs})]$	
$C_{\text{wtot}}$	<b>5.72E-20</b> Total water body COPC concentration, including water column and bed sediment (mg/L)
$L_T$	<b>4.86E-02</b> Total COPC load to the water body (including deposition, runoff, and erosion) (g/yr)
$Vf_w$	<b>1.32E+08</b> Average volumetric flow rate through water body (m <sup>3</sup> /yr)
$f_{wc}$	<b>7.95E-03</b> Fraction of total water body COPC concentration that occurs in the water column (unitless)
$f_{bs}$	$= [(1 + Kd_{bs} * TSS * 10^{-6}) * d_{bs}/d_z] / [(1 + Kd_{wc} * TSS * 10^{-6}) * d_{wc}/d_z + (Kd_{bs} * BS) * d_{bs}/d_z]$
$f_{bs}$	$= 1 - f_{wc}$
$f_{bs}$	9.92E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$Kd_{bs}$	6.27E+04 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-21 <sup>1</sup> )
TSS	3.00E+02 Total suspended solids concentration (mg/L)(High value for range listed in SLERA Protocol Table B-2-10 <sup>2</sup> )
	1.00E-06 Units conversion factor (kg/mg)
$d_{wc}$	4.05E-01 Depth of water column (m) <sup>3</sup>
$d_{bs}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-10)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-10, $d_z = d_{wc} + d_{bs}$ )
BS	1.00E+00 Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)
$\theta_{bs}$	6.00E-01 Bed sediment porosity ( $L_{\text{water}}/L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)
$Kd_{bs}$	3.34E+04 Bed sediment/sediment pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-21 <sup>1</sup> )
$k_{wt}$	<b>3.26E+10</b> Overall total water body COPC dissipation rate constant (yr <sup>-1</sup> ) <sup>4</sup>
$k_{wt} = f_{wc} * k_v + f_{bs} * k_b$	
$f_{wc}$	7.95E-03 Fraction of total water body COPC concentration that occurs in the water column (unitless)
$k_v$	1.20E+00 Water column volatilization rate constant (yr <sup>-1</sup> )
$f_{bs}$	9.92E-01 Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)
$k_b$	3.28E+10 Benthic burial rate constant (yr <sup>-1</sup> )
$A_w$	<b>5.98E+07</b> Water body surface area (m <sup>2</sup> )
$k_v$	<b>1.20E+00</b> Water column volatilization rate constant (yr <sup>-1</sup> )
$k_v = K_v / [d_z * (1 + Kd_{bs} * TSS * 10^{-6})]$	
$K_v$	1.03E+01 Overall COPC transfer rate coefficient (m/yr)
$d_{wc}$	4.05E-01 Depth of water column (m)
$d_{bs}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from Table B-2-12)
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-12, $d_z = d_{wc} + d_{bs}$ )
$Kd_{bw}$	6.27E+04 Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-21)
TSS	3.00E+02 Total suspended solids concentration (mg/L)
	1.00E-06 Units conversion factor (kg/mg)
$K_v$	<b>1.03E+01</b> Overall COPC transfer rate coefficient (m/yr)
$K_v = [K_L^{-1} + (K_G * H/(R * T_{wk}))^{-1}]^{-1} * q^{(T_{wk} - 29)}$	
$K_L$	6.18E+02 Liquid-phase transfer coefficient (m/yr)
$K_G$	3.65E+04 Gas-phase transfer coefficient (m/yr)
H	6.18E-06 Henry's Law constant (atm-m <sup>3</sup> /mol) (SLERA Protocol Table A-2-21)
R	8.21E-05 Universal gas constant (atm-m <sup>3</sup> /mol-K)
$T_{wk}$	2.98E+02 Water body temperature (K) (default value from SLERA Protocol Table B-2-13)
q	1.03E+00 Temperature correction factor (unitless) (default value from SLERA Protocol Table B-2-13)
$K_L$	<b>6.18E+02</b> Liquid-phase transfer coefficient for flowing streams or rivers (m/yr)
$K_L = \text{SQRT}(10^4 * D_w * u / d_z) * 3.1536 \times 10^7$	
$D_w$	5.49E-06 Diffusivity of COPC in water (cm <sup>2</sup> /s) (SLERA Protocol Table A-2-21)
u	3.05E-01 Current velocity (m/s) <sup>4</sup>
$d_z$	4.35E-01 Total water body depth (m) (Per SLERA Protocol Table B-2-14, $d_z = d_{wc} + d_{bs}$ )
	3.15E+07 Units conversion constant (s/yr)
$K_G$	<b>3.65E+04</b> Gas-phase transfer coefficient for flowing streams or rivers (m/yr) (default value from SLERA Protocol Table B-2-15)
$k_b$	<b>3.28E+10</b> Benthic burial rate constant (yr <sup>-1</sup> )
$k_b = [X_e * A_L * SD * 10^3 - Vf_w * TSS / (A_w * TSS)] * [TSS * 10^{-6} / (BS * d_{bs})]$	
$X_e$	2.54E+01 Unit soil loss (kg/m <sup>2</sup> -yr)
$A_L$	1.51E+09 Total watershed area receiving COPC deposition (m <sup>2</sup> )
SD	8.55E-02 Watershed sediment delivery ratio (unitless)
$Vf_w$	1.32E+08 Average volumetric flow rate through water body (m <sup>3</sup> /yr)
TSS	3.00E+02 Total suspended solids concentration (mg/L)
$A_w$	5.98E+07 Water body surface area (m <sup>2</sup> )
BS	1.00E+00 Benthic solids concentration (g/cm <sup>3</sup> ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-16)
$d_{bs}$	3.00E-02 Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-16)

Notes:

<sup>1</sup> Assume pH = 6.8 based on USGS data on Casey Fork near Mount Vernon

<sup>2</sup> No data available for location of deposition, therefore used high end of SLERA default range.

<sup>3</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

<sup>4</sup> Assumed based on USGS data from Casey Fork near Mount Vernon.

**Table B6-5. Benzo(b)fluoranthene Concentration in Water Column**

$C_{wctot} = f_{wc} * C_{wtot} * (d_{wc} + d_{bs}) / d_{wc}$		
<b><math>C_{wctot}</math></b>	<b>4.89E-22</b>	Total COPC concentration in water column (mg/L)
$f_{wc}$	7.95E-03	Fraction of total water body COPC concentration that occurs in the water column (unitless)
$C_{wtot}$	5.72E-20	Total water body COPC concentration, including water column and bed sediment (mg/L)
$d_{wc}$	4.05E-01	Depth of water column (m)
$d_{bs}$	3.00E-02	Depth of upper benthic sediment layer (m) (default value from SLERA Protocol Table B-2-17)

**Table B6-6. Benzo(b)fluoranthene Dissolved Phase Water Concentration**

$C_{dw} = C_{wtotal} / (1 + Kd_{sw} * TSS * 10^{-6})$		
$C_{dw}$	<b>2.47E-23</b>	Dissolved phase water concentration (mg/L)
$C_{wtotal}$	<b>4.89E-22</b>	Total COPC concentration in water column (mg/L)
$Kd_{sw}$	<b>6.27E+04</b>	Suspended sediments/surface water partition coefficient (L/kg) (SLERA Protocol Table A-2-21)
TSS	<b>3.00E+02</b>	Total suspended solids concentration (mg/L)

**Table B6-7. Benzo(b)fluoranthene Concentration in Bed Sediment**

$C_{\text{sed}} = f_{\text{bs}} * C_{\text{wtot}} * [Kd_{\text{bs}} / (\theta_{\text{bs}} + Kd_{\text{bs}} * BS)] * [(d_{\text{wc}} + d_{\text{bs}}) / d_{\text{bs}}]$				
<b><math>C_{\text{sed}}</math></b>	<b>8.24E-19</b>	COPC concentration in bed sediment (mg/kg)		
<b><math>f_{\text{bs}}</math></b>	<b>9.92E-01</b>	Fraction of total water body COPC concentration that occurs in the benthic sediment (unitless)		
<b><math>C_{\text{wtot}}</math></b>	<b>5.72E-20</b>	Total water body COPC concentration, including water column and bed sediment (mg/L)		
<b><math>Kd_{\text{bs}}</math></b>	<b>3.34E+04</b>	Bed sediment/pore water partition coefficient (L/kg) (SLERA Protocol Table A-2-21)		
<b><math>\theta_{\text{bs}}</math></b>	<b>6.00E-01</b>	Bed sediment porosity ( $L_{\text{water}} / L_{\text{sediment}}$ ) (default value from SLERA Protocol Table B-2-10)		
<b><math>BS</math></b>	<b>1.00E+00</b>	Benthic solids concentration ( $\text{g/cm}^3$ ) (equivalent to kg/L) (default value from SLERA Protocol Table B-2-10)		
<b><math>d_{\text{wc}}</math></b>	<b>4.05E-01</b>	Depth of water column (m)*		
<b><math>d_{\text{bs}}</math></b>	<b>3.00E-02</b>	Depth of upper benthic sediment layer (m) (default value from Table B-2-12)		

**Table B7-1. Benzo(k)fluoranthene Summary**

	Concentration from Project	Background Concentration <sup>1</sup>	Total Concentration (Background & Project)	Ecological Screening Level <sup>2</sup>	Toxicity Reference Value <sup>3</sup>	Total Concentration Percent of ESL	Ecological Screening Quotient
Soil (mg/kg)	6.77E-08	1.00E+01	1.00E+01	1.48E+02	2.50E-01	6.76%	N/A
Water (mg/L)	4.20E-21	N/A	N/A	N/A	2.70E-05	N/A	0.00
Sediment (mg/kg)	7.09E-18	N/A	N/A	2.40E-01	3.70E-02	N/A	0.00

Notes:

<sup>1</sup> Soil background concentration obtained from USGS survey of the area around Chicago, IL; Kay, R.T., et al, Concentrations of Polynuclear Aromatic Hydrocarbons and Inorganic Constituents in Ambient Surface Soils, Chicago, Illinois: 2001-2002. United States Geological Survey, 2003.

<sup>2</sup> U.S. EPA Region 5 Waste Division, RCRA Corrective Action Guidance and Policy Documents, Ecological Screening Levels, August 22, 2003 available at <http://www.epa.gov/region5/cara/ca/guidance.htm>.

<sup>3</sup> U.S. EPA, Office of Solid Waste. Screening Level Ecological Risk Assessment Protocol for Hazardous Waste Combustion Facilities, Volume 1. EPA 530-D-99-001A. August 1999.